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# PHASE II--INDUSTRIAL AREA GROUNDWATER REPORT ALABAMA ARMY AMMUNITION PLANT

# Prepared by:

ENVIRONMENTAL SCIENCE AND ENGINEERING, INC. 11665 Lilburn Park Road St. Louis, Missouri 63141

> FINAL REPORT 30 November 1981

> > Prepared for:

U.S. ARMY TOXIC AND HAZARDOUS MATERIALS AGENCY
Aberdeen Proving Ground, Maryland 21010

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#### EXECUTIVE SUMMARY

This report summarizes the findings of the Phase II survey of the geohydrological characteristics and water quality of the water-table aquifer underlying the Industrial Area and the Flashing Ground at Alabama Army Ammunition Plant (AAAP), Childersburg, Alabama. During the period October 1979 to October 1980, an environmental survey (Phase I) of AAAP was conducted by Environmental Science and Engineering, Inc. (ESE) under contract to the U.S. Army Toxic and Hazardous Materials Agency (USATHAMA). The results of the Phase I survey reported by ESE (1981) indicated that the water-table aquifer underlying these areas was contaminated by nitroaromatic residues as a result of past industrial operations.

As a consequence of the potential for contaminant migration off site, further studies were performed to more clearly define the zone of contamination and extent and direction of contaminant movement. These further studies comprise the Phase II groundwater survey.

Thirty monitor wells were constructed during Phase I. Data gathered from these wells have been reported by ESE (1981). During Phase II, an additional II wells were constructed along with two piezometer clusters to further define the characteristics of the water-table aquifer and the potential for vertical migration. Thirteen slug tests were performed to assess horizontal permeabilities. During Phase I, samples from 26 wells were analyzed to define the water quality characteristics of the water-table aquifer. During Phase II, samples from all of the newly constructed wells were analyzed along with samples from each of the 7 wells in which contamination had been observed during Phase I.

Based on the Phase I data reported by ESE (1981) and the Phase II data presented in this report, the contamination status and migration potential have been described. The major conclusions are as follows:

- 1. The results of the Phase I and Phase II studies indicate that the water-table aquifer underlying the Industrial Area at AAAP contains pockets of nitroaromatic contamination which appear to be localized near discrete sources of soil contamination. These include the sites of the Washer-Flaker Houses within the Southern and Northern TNT Manufacturing Areas and contaminated spoil banks lining the Red-Water Ditch in the Southern TNT Manufacturing Area. Contaminated sediments from AAAP surface water bodies themselves do not appear to contribute significantly to the groundwater contamination. The presence of tetryl in the ground water was confirmed in the sample from only one well during Phase II. Based on the Phase I and Phase II data, the horizontal extent of contaminated ground water from these past industrial activities is confined to the Industrial Area.
- 2. At the Flashing Ground, nitroaromatic contamination of the ground water was not detected during Phase II and was observed only at the analytical detection limit during Phase I. Most of the groundwater constituents were observed to be at lower concentrations during Phase II due to antecedent rainfall conditions. Small peaks were observed in the Phase II chromatograms, but these were below the detection limits. Only small amounts of contaminants are migrating horizontally downgradient at this location as leachate from the contaminated soil.
- 3. Nitroaromatic concentrations were diluted during Phase II as a result of antecedent rainfall conditions as indicated by the comparative Phase I and Phase II data. The major contaminants found during both surveys were 2,4,6-trinitrotoluene; 2,4- and

2,6-dinitrotoluene, 1,3-dinitrobenzene, and 1,3,5-trinitrobenzene.

During Phase I (ESE, 1981), several other nitroaromatic compounds, transformation products of trinitrotoluene, were identified in the sample from the most heavily contaminated well (Well P-10). These were 4-amino-2,6-dinitrotoluene, 3,5-dinitroaniline, 2-amino-4,6-dinitrotoluene, 2,4-dinitrophenol, and 2-methyl-4,6-dinitrophenol. These compounds are found in trinitrotoluene manufacturing wastewater and also have been identified as transformation products in trinitrotoluene degradation. These transformation products were detected in Well P-10 by GC/MS screening and, with the exception of 2,4-dinitrophenol, were observed at concentrations an order of magnitude less than 2,4,6-trinitrotoluene, 2,4-dinitrotoluene, and 1,3,5-trinitrobenzene. Their presence would be expected in each of the other wells, but at levels far below detection limits.

- 4. The general direction of horizontal movement of the ground water in the water-table aquifer underlying the Industrial Area is toward the Coosa River regionally and toward the Red-Water Ditch and Beaver Pond drainage system locally, with a horizontal gradient of approximately 0.01 meter per meter. Horizontal movement rate was calculated to be approximately 2.9 meters per year in this area.
- 5. Based on the above and the downgradient distance from the nearest contaminated well (Well P-11) to the AAAP boundary, contamination in the water-table aquifer in the Industrial Area will take a total of approximately 230 years to reach the boundary.
- At the Flashing Ground, the water table slopes to the southeast toward Talladega Creek at a gradient of 0.0275 meter per meter.

The horizontal movement rate was calculated to be 7.7 meters per year.

- 7. Because of the proximity to the AAAP boundary and steep groundwater gradient, the time required for contaminants to migrate to the boundary is approximately 3 years.
- 8. Recharge of the lower aquifer (dolomitic limestone bedrock)
  was calculated to occur at a rate of 95 liters per year per
  square meter in the Industrial Area. This is equivalent to a
  vertical migration rate of 0.23 meter per year. Contaminated
  ground water would require approximately 10 years to migrate to
  the lower aquifer from contaminated pockets in the Northern TNT
  Manufacturing Area and approximately 33 years from contaminated
  pockets in the Southern TNT Manufacturing Area.

#### 1.0 INTRODUCTION

#### 1.1 BACKGROUND

AAAP was constructed during World War II to produce high explosives, smokeless powder, and nitrocellulose for the war effort. After the war, the facilities were retained on standby status until 1973 when they were declared excess to U.S. Army requirements and partially razed.

An environmental survey of AAAP was conducted by ESE under contract to USATHAMA from September 1979 to October 1980. This first phase survey, which involved investigation of the entire 5,168 acres (2,088 hectares), included a groundwater investigation based on sampling and analysis of 30 monitor wells. A summary of the results of the Phase I groundwater analysis (ESE, 1981) is presented below.

The water table aquifer underlying the Industrial Area is contaminated by nitroaromatic residues and shows evidence of impact from inorganic salts. Two wells, one located in each of the TNT manufacturing areas, contained water more highly contaminated than the water in other wells in the Industrial Area, indicating that the TNT manufacturing areas are the source of the groundwater contamination. One well, located in the Southern TNT Manufacturing Area, contained water of a bright yellow color. This water contained approximately 21 ppm nitroaromatic residues. The principal compounds were trinitrotoluene, 2,4-dinitrotoluene, 2,6-dinitrotoluene, 1,3-dinitrobenzene, 1,3,5-trinitrobenzene, 2,6-dinitrophenol, and 2-methyl-4,6-dinitrophenol. The second-most contaminated well, located in the Northern TNT Manufacturing Area. contained approximately 135 ppb of total nitroaromatic residues.

The potentiometric surface of the water table aquifer and the conductivity of the water in this aquifer indicate the presence of significant sources of dissolved solids in both the Southern and Northern TNT Manufacturing Areas, the Acid/Organic Manufacturing Area, the Red-Water Storage Basin, and the west side of the Tetryl Manufacturing Area. A groundwater plume with dissolved solids concentrations above

background levels appears to follow the Red-Water Ditch drainage system toward the Coosa River. The Red-Water Ditch was the principal conveyor of industrial wastewaters during plant operations.

The water table aquifer at the Flashing Ground located in the southeast corner of AAAP contains traces of 2,4-dinitrotoluene (3.6 ppb) apparently derived from the soils of that disposal area. While this concentration level is low, the proximity of the Flashing Ground to the installation boundary indicates potential off-post migration.

#### 1.2 STUDY OBJECTIVES

One purpose of the Phase II study was to provide the information necessary to develop impact mitigation plans for the Industrial Area and the Flashing Ground (Study Area 16). To meet this objective, the groundwater-specific tasks were designed to:

- 1. Define more precisely the extent of groundwater contamination,
- 2. Estimate the rate and direction of groundwater movement, and
- Determine if there is any significant off-site migration of hazardous materials.

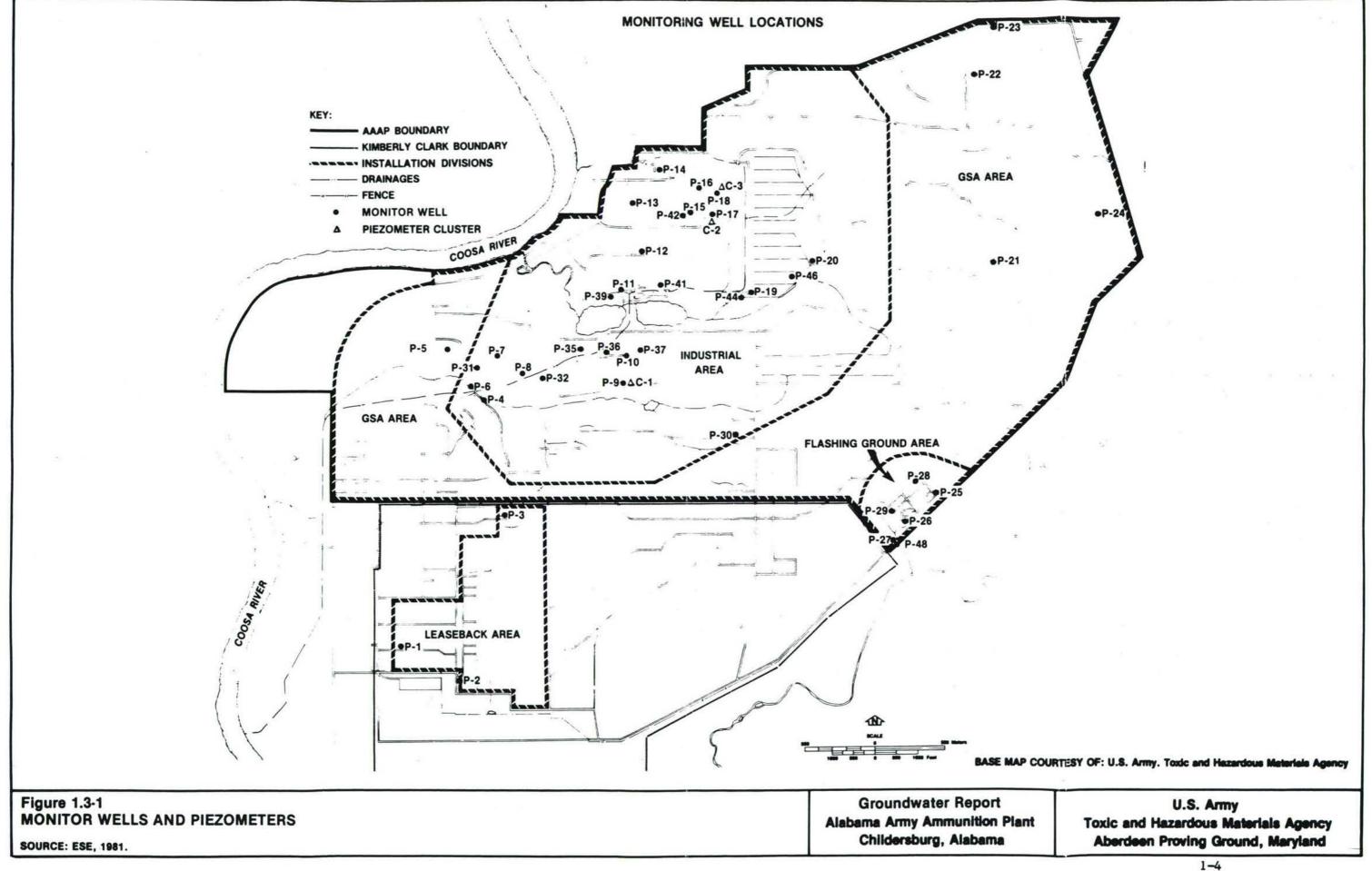
In the Industrial Area, seven additional wells and two piezometer clusters were installed to further investigate the water-table aquifer. Water samples were collected from these new wells, plus all wells previously reported to be contaminated, and were analyzed for nitroaromatic compounds. Hydraulic tests were performed on selected wells to determine the rate and direction of groundwater movement.

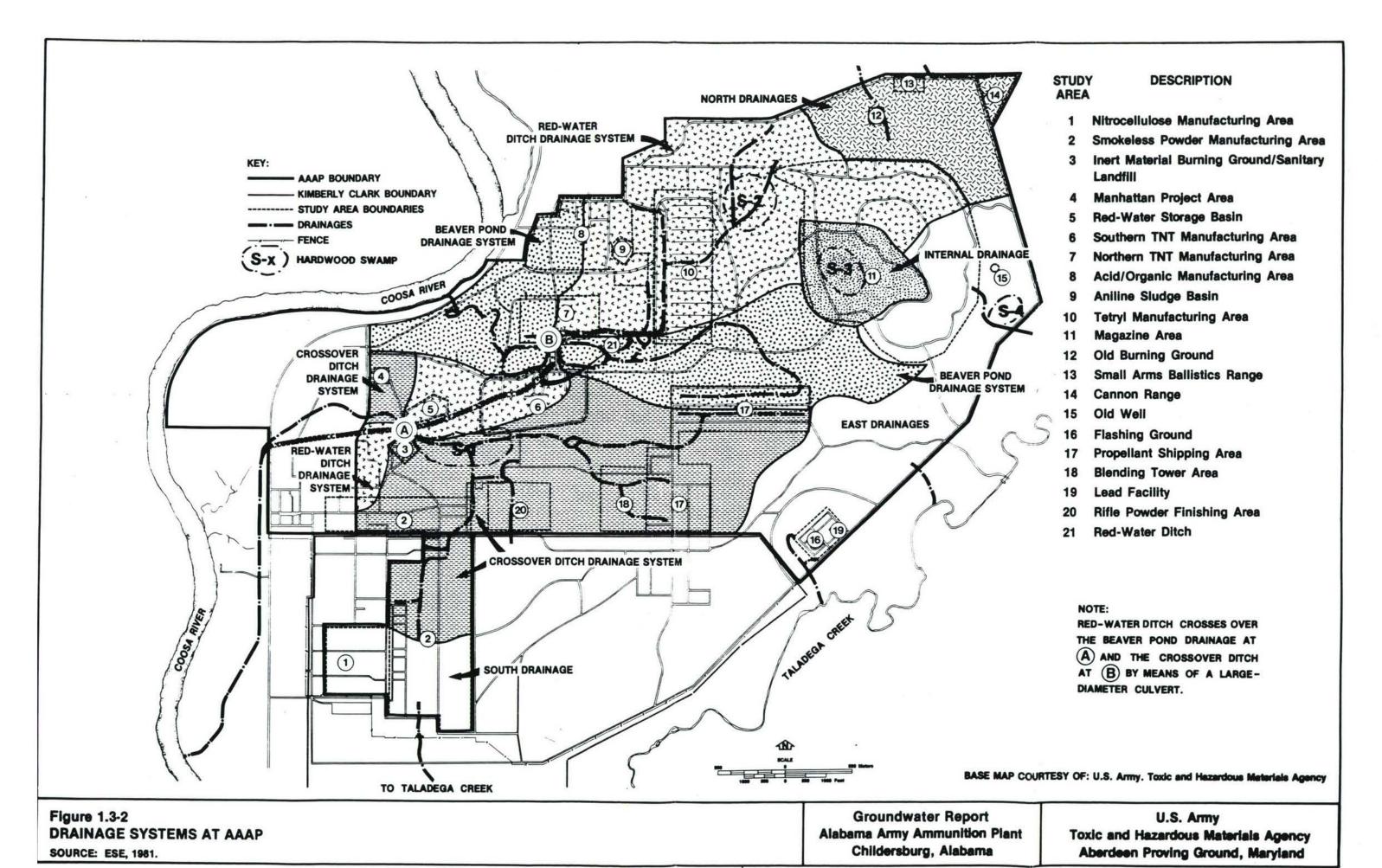
One new monitor well (Well P-48) was installed in the drainageway downgradient of the Flashing Ground near the southeast property boundary. Water samples from two wells in this area were analyzed to determine the off-site movement of contaminants.

#### 1.3 SITE SELECTION

Figure 1.3-1 shows the location of all the wells drilled at AAAP;
Figure 1.3-2 identifies the major surface drainage systems and water
bodies at AAAP. Wells P-1 through P-30 were constructed as part of
Phase I (Environmental Survey). Wells P-31 through P-48 and piezometer
locations C-1, C-2, and C-3 were constructed for Phase II. Although
monitor wells are numbered P-1 through P-48, only 41 wells were actually
installed; 7 wells were eliminated during the planning phase, and the
numbers were not reallocated to avoid confusion in the field program.

Of the original 30 wells sampled and analyzed during Phase I, only 7 (Wells P-2, P-6, P-10, P-11, P-15, P-19, P-20) contained detectable levels of explosives-derived chemicals. The general principle used in site selection for the additional wells constructed in Phase II was to place at least one well downgradient (where possible) from each contaminated well to attempt to determine the extent of contaminant migration. Additional wells were located upgradient of wells known to be contaminated and at other selected locations to further define the water-table characteristics. Table 1.3-1 is a listing of the new wells and the rationale for their site selection.





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Table 1.3-1. Additional Monitor Wells and Piezometers (Locations Shown on Figure 1.3-1)

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Well	Location	Rationale
P-31	Near the northwest corner of the Red-Water Storage Basin (Study Area 5)	Clarify the groundwater flow direction near Wells P-6 and P-7 and determine if contaminants have moved in that direction.
P-32	Adjacent to the Red-Water Ditch (Study Area 21)	Define the relationship between the Red-Water Ditch and the water table.
P-35	Near the end of TNT Manufacturing Line F, downgradient of Well P-10 and the Red-Water Ditch	Determine groundwater elevation and monitor contaminants.
P-36	Downgradient of Well P-10 adjacent to Red-Water Ditch	Monitor the groundwater elevation and measure the extent of contaminant migration.
P-37	At the end of TNT Manufacturing Line H, immediately upgradient of Well P-10	Determine groundwater elevation and monitor contamination.
P-39	Downgradient of Well P-11	Determine groundwater elevation and monitor contamination.
P-41	Near the end of TNT Manufacturing Line F	Determine groundwater elevation and monitor contamination.
P-42	Downgradient of Well P-15	Determine groundwater elevation and monitor contamination.
P-44	Downgradient of Well P-19	Determine groundwater elevation and monitor contamination.

Table 1.3-1. Additional Monitor Wells and Piezometers (Locations Shown on Figure 1.3-1) (Continued, Page 2 of 2)

Well	Location	Rationale
P-46	Downgradient of Well P-20	Determine groundwater elevation and monitor contamination.
P-48	Downgradient of Well P-26	Determine if groundwater contaminants are migrating off site.
Piezometer Cluster C-1	Near Well P-9, upgradient of Well P-10	Monitor vertical head gradients.
Piezometer Cluster C-2	Near Well P-17, at south end of Aniline Sludge Basin (Study Area 9)	Monitor vertical head gradients. (Subsurface conditions forced abandorment of this cluster.)
Piezometer Cluster C-3	Near Well P-18, upgradient of Aniline Sludge Basin (Study Area 9)	Monitor vertical head gradients.

#### 2.0 FIELD METHODS

#### 2.1 WELL DESIGN AND CONSTRUCTION

#### 2.1.1 MONITOR WELLS

All monitor wells were designed and constructed according to the specifications provided in USATHAMA's "Minimal Requirements for Boring Logs, Monitor Well Sketches, and Drilling Operations." Wells P-31 to P-47 (see Figure 2.1-1) were constructed in the following manner:

- An 8-inch borehole was drilled, using hollow-stem augers, to a
  depth of 4.6 meters (15 feet) below the water table, or to
  apparent bedrock, with a maximum depth of 15.3 meters (50 feet).
  Split-spoon samples were taken every 1.5 meters (5 feet); grab
  samples were taken at any level where a change in lithology was
  noted.
- 2. The top of the well screen [typically 6.1 meters (20 feet) of factory-slotted, 4-inch, Schedule 40 PVC screen with a slot width of 0.010 inch] was set at 1.5 meters (5 feet) above the water table noted during drilling.
- The well casing extended approximately 0.6 meter (2 feet) above the ground surface.
- 4. The filter pack of fine to medium sand was placed in the annular space to a depth approximately 0.6 meter (2 feet) above the top of the well screen.
- 5. Approximately 1 meter (3 feet) of pelletized bentonite seal was placed on top of the filter pack; thus, the top of the bentonite seal extended 1.6 meters (5 feet) above the top of the well screen.
- 6. The annular space from the top of the bentonite seal to the land surface was grouted with a mixture of Portland cement, sand, and water. The mixture was approximately 2 parts dry-weight sand to 1 part cement with not more than 7 gallons of clean water per 94-pound bag of cement.

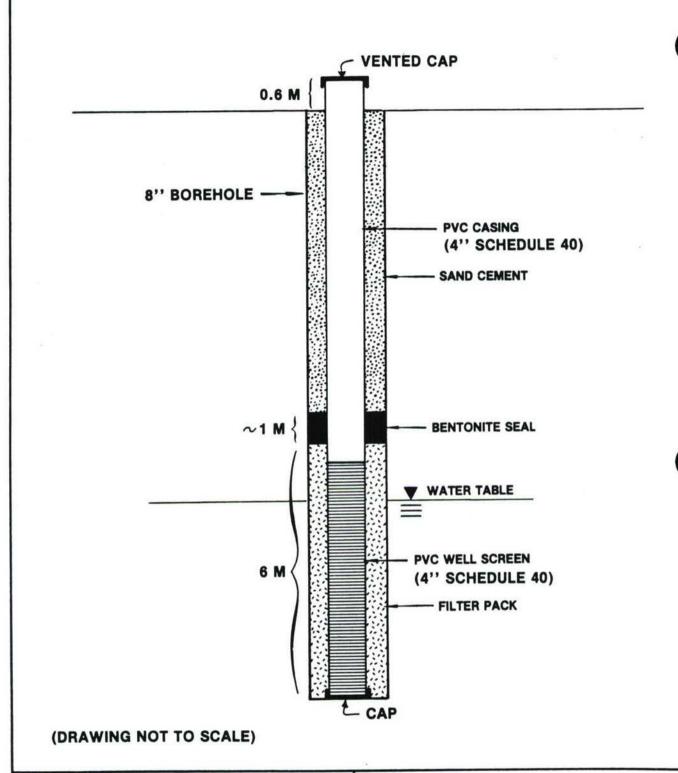


Figure 2.1-1

TYPICAL CONSTRUCTION DETAIL OF WELLS P-31 THROUGH P-47

SOURCE: ESE, 1981.

Groundwater Report
Alabama Army Ammunition Plant
Childersburg, Alabama

U.S. Army
Toxic and Hazardous Materials Agency
Aberdeen Proving Ground, Maryland

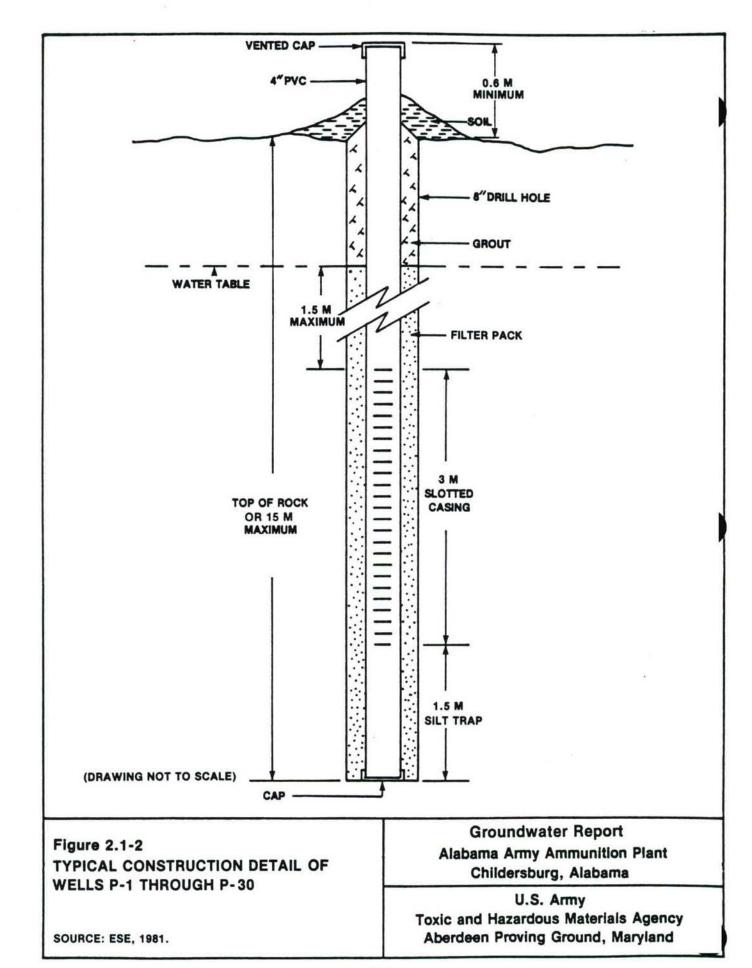
- 7. The well was developed by surging and bailing for approximately 1 hour.
- Each well was marked with a flagged, 2-meter (6-foot) steel post.
- USATHAMA's Contracting Officer waived the requirement for protective casing on the water-table monitor wells.
- 10. After installation, well locations were surveyed to a horizontal accuracy of +0.3 meter (+1 foot). The top of the well casing was surveyed to +0.03 meter vertically. Benchmarks used were U.S. Army Corps of Engineers benchmarks on the AAAP site located at installation coordinates 22,000-N/10,800-E and 22,800-N/14,000-E.

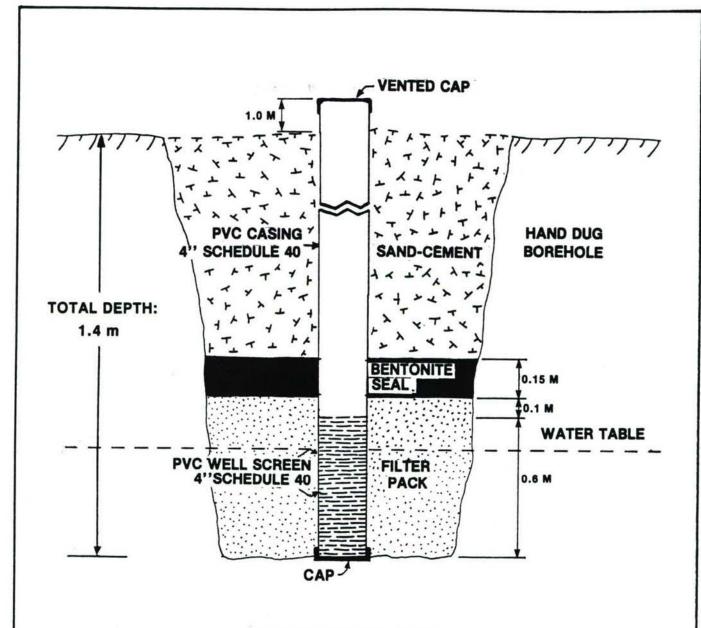
Construction of Wells P-1 through P-30 (shown in Figure 2.1-2) was similar to construction of Wells P-31 through P-47 except:

- The screen in Wells P-1 through P-30 terminated no farther than
   1.5 meters (5 feet) from the water table:
- A bentonite seal was used in Wells P-31 through P-47, and sand-cement grout was placed from the water table to the surface;
- The screen was 3 meters (10 feet) in length in Wells P-1 through P-30;
- 4. A silt trap was included at the bottom of several wells (Wells P-1 through P-30) in the first series.

Because the steep terrain below the Flashing Ground limited drilling rig access, Well P-48 was constructed by hand in the drainageway leading off site. Details of the construction of this well are shown in Figure 2.1-3.

During the drilling operation, subsurface soil samples were collected from the monitoring wells. Soil samples were taken at least every 1.5 meters (5 feet) during drilling by ASTM Method D1586-67 (Standard Penetration Test); additional samples were taken when a significant





(DRAWING NOT TO SCALE)

Figure 2.1-3
CONSTRUCTION DETAIL OF WELL P-48

Groundwater Report Alabama Army Ammunition Plant Childersburg, Alabama

SOURCE: ESE, 1981.

U.S. Army
Toxic and Hazardous Materials Agency
Aberdeen Proving Ground, Maryland

stratigraphic change was noted. All of the subsurface soil samples have been retained for future reference or analysis until completion of the contract.

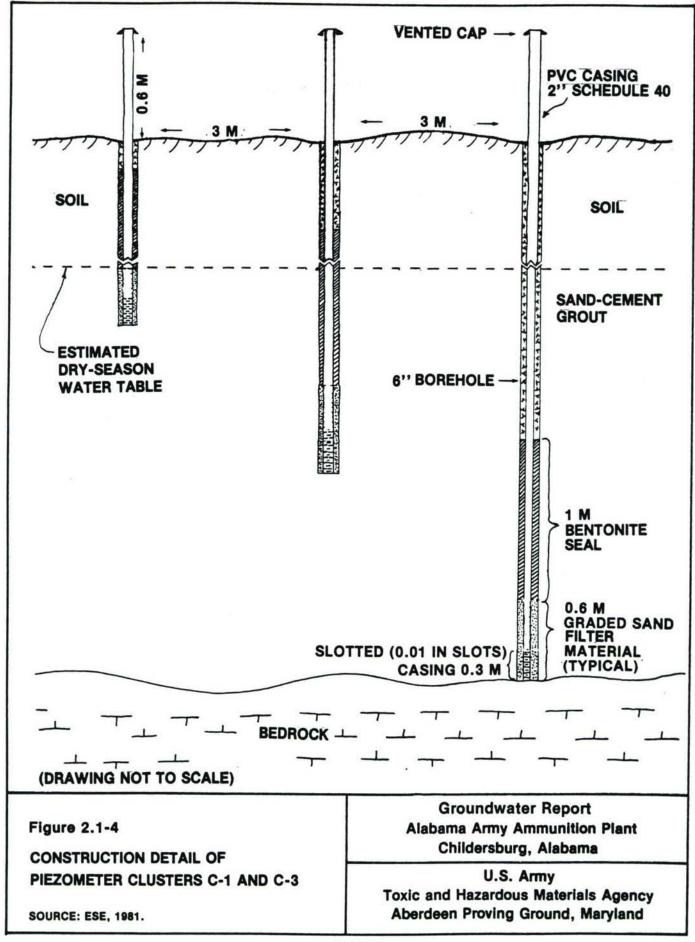
Detailed well logs were prepared showing stratigraphic and lithologic details of the materials present in the hole. All soil descriptions were made in accordance with the Unified Soil Classification and soil colors identified by the Munsell Soil Color Chart. Original copies of the well logs were delivered to USATHAMA at completion of each well. Field drilling files for Phase I and Phase II are included in Appendix C and Appendix D, respectively.

#### 2.1.2 PIEZOMETER CLUSTERS

Two clusters (C-1 and C-3) of three piezometers each were installed during this study. Each cluster was designed to measure the water pressure (represented as elevation) in a particular stratum. When three piezometers (one deep, one medium, and one shallow) are installed adjacent to each other, the water level in each describes the hydraulic pressure at that depth. If water levels are different in any of the piezometers, it is an indication that potential exists for fluid migration from the higher to lower pressure zones. These clusters were used to assess the potential for vertical groundwater movement.

Piezometer Clusters C-1 and C-3 were installed near Wells P-9 and P-18, respectively, as shown on Figure 1.3-1. During the construction of Piezometer Cluster C-2, geological problems were encountered (refer to Section 2.4.2).

Construction details of the piezometer clusters are presented in Figure 2.1-4. The deepest piezometer in each cluster (average 14.3 meters deep) was constructed first to log the complete geological section to apparent bedrock and determine the thickness of the soil at that point. The shallowest piezometer (average 6.1 meters deep) was



installed just below the estimated dry season water table. The third piezometer was placed at mid-depth between the other two.

## 2.2 GROUNDWATER SAMPLING

Groundwater samples were collected on February 25, 1981. Prior to sampling, each well was bailed to ensure that the sample collected was representative of the native ground water. The bailing was continued until five well volumes were removed, unless the well was bailed dry before five volumes had been removed. For some of the slow-recovery wells, only two well volumes were removed prior to sampling.

All water-level measurements (except slug tests) were made either with electric tape instruments or with conventional steel tape. Water levels were recorded from the top of the casing. Water-level elevations were then calculated. Land survey data were referenced to the top of the casing. Measurements made as part of the sampling effort were made prior to bailing. The tape was cleaned between measurements to prevent cross contamination.

To prevent cross-contamination of the wells during development and sampling, individual bailers which remained in place at every well were fabricated. These bailers were economically constructed of PVC with a plastic ball used as a valve at the bottom. As an additional protective measure, polyethylene sheeting was laid around the well head whenever the bailer was raised to prevent contact between the bailer or its support line and potentially contaminated soil.

Groundwater samples were collected and filtered through a 0.45-um membrane filter within a maximum of 4 hours after collection. However, several samples that were too turbid to be filtered in the field were centrifuged and filtered at the ESE Gainesville laboratory. The following is a list of the wells which were filtered and those which could not be filtered on site.

Wells Filtered On Site	Wells Filtered at ESE Laboratory
P-19	P-6
P-20	P-10
P-23	P-11
P-26	P-15
P-32	P-31
P-39	P-35
P-42	P-36
P-44	P-37
P-46	P-41
	P-48

Specific conductivity and pH were measured immediately after collection. Samples were kept chilled and protected from sunlight during processing. After filtration, the samples were preserved and packed in ice-filled chests at AAAP. Analytical results are presented and discussed in Section 4.2.

#### 2.3 HYDRAULIC TESTING

Groundwater flow, which essentially controls contaminant migration, depends on several factors, including permeability of the aquifer. Because of the contaminated status of wells in the Industrial Area, hydraulic tests known as slug tests were performed on eight monitor wells in this area. Analysis of the slug test data has enabled ESE to define the hydraulic conductivity and permeability of the water-table aquifer. These values, in conjunction with soils data and water-table measurements, have been used to make estimates of groundwater flow rates and directions of movement (see Section 4.1.2).

The slug test is generally used in single-well situations where the permeability of the surrounding soils is too low to run a conventional pump test. During a slug test, a known volume of water (slug) is instantaneously displaced (added or removed), and a record is made of the time required for the water level to return to equilibrium. These

data are then analyzed to yield values of permeability. Because the volume of water displaced during slug tests is small, the permeability values determined are only representative of the soils in the immediate proximity (within a few meters) of the well. Therefore, it is important to make a number of tests in the area to ensure that the values adequately characterize the area.

During field testing, the time-rate relationship of water-level changes was recorded by a Paroscientific® quartz pressure sensor (QPS) and dedicated battery-powered digital signal processor (DSP). The pressure sensor is designed to fit into a 3-inch well and is capable of recording pressure variations of 0 to 900 pounds per square inch (psi) (2,000-foot head variations) with 0.001 psi resolution. The water level was displaced by a 3.5-inch outside diameter (0.D.) Schedule-40 PVC mechanical slug which was approximately 8 feet (2.4 meters) long. The PVC slug was used to displace a known volume of water in the well. The results obtained using this procedure are identical to those obtained by adding or removing a "slug" of water to or from the well. The advantages of using a PVC slug are that potentially contaminated water is not removed from the well and nontypical water is not added to the well. Between tests, the PVC slug was thoroughly cleaned to prevent cross-contamination between wells.

The testing procedure was to record the initial depth to water with an electric tape to determine the volume of water in each well, then lower the QPS to a depth near the bottom of the well. Because the QPS displaced some water volume, the level was allowed to come to equilibrium as recorded by the DSP. Next, the slug was quickly lowered into the well (slug-in test) and pressure measurements were recorded at short, timed intervals (1 second to several minutes) until the water again returned to equilibrium.

After completion of the slug-in test, the slug was quickly removed (slug-out test), and the recording procedure was repeated as a slug-out

test to determine the response function of the well under rising pressure head conditions.

Analysis of the slug test data was based on the method described by Bouwer and Rice (1976). This procedure was selected because it makes allowances for field situations at AAAP where the aquifer is not under artesian conditions and the wells do not fully penetrate the aquifer. The analysis assumes that the aquifer and therefore the coefficient of permeability are uniform over the entire thickness tested. Also, this method takes into account the porosity difference between the filter pack and the aquifer.

Field data for each test were tabulated as elapsed time (t) and change in pressure  $(\Delta p)$ , which were plotted on semi-log graphs (t on the arithmetic scale,  $\Delta$ p on the logarithmic scale). Graphs of all wells tested are presented in Appendix A. Hydraulic conductivity was calculated according to the Bouwer and Rice (1976) equation:

$$K = \frac{r_c^2 \ln (R_e/r_w)}{2L} \frac{1}{t} \frac{\ln \frac{Y_o}{Y_t}}{\frac{1}{t}}$$

K = Hydraulic conductivity, in feet per second (reported as centimeters per second);

= Radius, in feet; derived from the actual radius of

the casing and the porosity and thickness of the filter pack; \* radius of well section when water filter pack; \* fewel is visions. See opp. page Re = Re-effective radius, in feet; must be solved for using equations and a graph presented in the original affective radial distance our when the history paper; affective is chargeful.

rw = Well radius, in feet; rockal dictance between well center and unclistuated aquifer.

L = Length of screen, in feet; re plus think ness analy.

t = Time, in seconds;

Yo = Pressure at y-intercept on graph, in psi; and

Yt = Pressure at time t, in psi.

Hydraulic conductivity was determined for all the slug-in (SI) tests and for selected slug-out (SO) tests. Slug-out data for several of the wells are not presented because analysis of the slug-in data indicated that the well had not recovered entirely to equilibrium before the slug-out tests were made. Therefore, any data from these slug-out tests are invalid. Results are tabulated in Table 2.3-1. Work sheets explaining the detailed calculations for each tested well are presented in Appendix A.

The permeability values measured in the majority of the wells  $(10^{-3} \text{ to } 10^{-6} \text{ cm/sec})$  are typical of the range of values reported by standard textbook references for mixtures of sand, silt, and clay found at AAAP. The primary reason for the range of values is variations in soil type. Minor variations in sand or silt content, as well as slight changes of compaction, can account for this range of permeabilities. The soils at AAAP show considerable variation from well site to well site, which accounts for the variation of permeability rates.

Well P-11 yielded a permeability rate (10<sup>-1</sup> cm/sec) considerably outside of the range normally expected in sandy clay soil. This high value indicates the presence of a more permeable zone, although none was reported on the drilling logs. There are two possible explanations for this occurrence. First, even a very small sand lens would conduct a volume of water many times greater than would normally be transmitted by a well surrounded by all clay soil.

The other possibility is that, in areas where clay soils overlie limestone bedrock, a weathered zone often exists immediately on top of the limestone. If this zone consists primarily of rock fragments, or if significant solution features exist at the soil-rock interface, the permeability at the interface will be higher than the permeability of the soil or the rock. The well casing is reported by field notes to be set on bedrock (refusal, by blow count determination) which may be in direct hydraulic contact with the bedrock aquifer. Water-level data

Table 2.3-1. Slug Test Summary

Well	Permeability (cm/sec)	
Number	Slug-In Test	Slug-Out Test
P-6	2.4 x 10 <sup>-6</sup>	
P-10	$8.1 \times 10^{-4}$	$3.7 \times 10^{-4}$
P-11	0.76	0.30
P-26	$6.4 \times 10^{-4}$	
P-35	$2.0 \times 10^{-3} \times 3.4 \times 10^{-4} \uparrow$	
P-37	4.4 x 10 <sup>-5</sup>	
P-41	$3.9 \times 10^{-3}$	$1.6 \times 10^{-3}$
P-44	$5.3 \times 10^{-5} \times 1.5 \times 10^{-4} \uparrow$	
Range	0.30 to 2.4 x 10	6

<sup>\*</sup> Early time.

Note: The different permeability values calculated for early and late times indicate changes in soil characteristics near the tested well. At Well P-35, the higher value indicates that a more permeable soil zone exists near the well, while the test of Well P-44 indicates the opposite.

Source: ESE, 1981.

<sup>†</sup> Late time.

from Well P-11 measured on February 11, 1981, show a water-level elevation within approximately 32 centimeters (1 foot) of that measured in the two deep piezometers C-1A and C-3A, which were constructed at bedrock surface.

If Well P-11 is hydraulically connected to a zone more permeable than the filter pack, the slug test results are actually representative of the filter pack material. The  $10^{-1}$  cm/sec rate determined in this test is similar to that reported for clean sands (Terzaghi, 1968) such as that used for the filter pack.

# 2.4 PROBLEMS ENCOUNTERED

# 2.4.1 DRILLING OF WELLS P-37 AND P-31

On the morning of January 16, 1981, the drilling team moved to the site of Well P-37 in the Southern TNT Manufacturing Area. The first attempted drilling terminated at 0.6 meter (2 feet) when the augers could not penetrate any farther. The drilling rig was moved approximately 3 meters (10 feet) to avoid the object which prevented drilling, probably a foundation.

The second attempt proceeded well except that the sandy clay soil was very hard (standard penetration blow counts greater than 50 per foot) at every 1.5-meter (5-foot) test interval. Several of the samples were a distinct purple color, not represented on the Munsell color chart. Throughout the rest of the AAAP site few soils required drilling rig blow counts of 50 per foot, and no other boring had consistent blow counts that high.

During the drilling, at about a 6-meter (20-foot) depth, an organic odor was noticed by the crew. When this odor was noticed, drilling was halted and a phone call was placed to the ESE Laboratory/Safety Officer. At that time, some crew members reported nausea and sore throats. On the following day, a faint aromatic odor was noted within 1.5 meters (5 feet) of the hole on the windward site. During the remaining work at

this well, the drillers and geologists were equipped with organic vapor masks to ensure their safety.

After discussion with the USATHAMA Project Officer, it was decided that the well should be constructed with a 0.6-meter (2-foot) clay seal at the bottom of the hole to prevent direct vertical movement of the ground water. However, as the augers were being withdrawn from the hole, approximately 1.7 meters (5.5 feet) of clay soil caved in at the bottom of the hole. A 0.3-meter (1-foot) bentonite seal was placed above this clay, and the well was completed in accordance with the Sampling and Analysis Plan (ESE, 1979).

In addition to the other difficulties encountered at Well P-37, a rope broke during the well development phase which allowed a 2-foot surge block to fall to the bottom of this well. After a lengthy attempt to retrieve this tool, it was decided by staff of both ESE and USATHAMA to abandon the effort. The presence of the surge block in this well does not hinder water sampling by the bailer methods. The surge block is constructed of a steel rod with a rubber belting material plunger. It does not contain any compounds which would interfere with analysis for nitroaromatic compounds.

A similar, but less severe, situation was encountered during construction of Well P-31 (near the west end of the Red-Water Storage Basin). At that location, the drillers experienced nausea, vomiting, and headaches. After a short period of time, they felt better, were issued vapor masks, and completed the well.

Since these incidents, all crew members [Pittsburgh Testing Laboratory, Inc. (PTL) drillers and the ESE geologists] have had full physical examinations which included blood tests. None of these tests indicated any disorder directly attributable to the type of chemicals encountered in the field.

#### 2.4.2 DRILLING OF PIEZOMETER CLUSTER C-2

Piezometer Cluster C-2 was planned for installation near Well P-17 at the southern end of the Aniline Sludge Basin (Study Area 9). The initial drilling proceeded in a typical manner. The soil encountered was sandy clay with medium blow counts to a depth of about 7.6 meters (25 feet), where no sample was recovered. An interval of no split-spoon sample recovery is not uncommon when sampling soil materials that exhibit low cohesive strengths (such as wet sands) or cohesive soils with water contents at or near the liquid limit. After another attempt at collecting a sample at the 7.6-meter (25-foot) depth, the hollow-stem augers were advanced to 9 meters (30 feet) and then 10.7 meters (35 feet), and additional attempts were made to collect a sample. The weight of the drill rods pushed the sampler to a depth of approximately 20.7 meters (68 feet). While the split spoon rested on the bottom, the 140-pound hammer was used to attempt to make a penetration test. No penetration had been made after 100 blows, indicating refusal. The sound of the equipment indicated a very solid base (probably rock). During the drilling, the driller did notice a change in drilling resistance at a depth of 8.4 meters (27.5 feet).

The following morning, after considerable discussion with the USATHAMA geologist, it was decided to pull the hollow-stem augers and construct the best well possible under the conditions encountered. A section of well screen 0.3 meter (1 foot) long was attached to the casing and pushed into the hole to a depth of approximately 13 meters (43 feet). At that depth, considerable resistance was encountered, and to avoid breaking the screen, the insertion effort was halted.

The well was developed and then sealed with bentonite and concrete. Later measurements of water-level fluctuations in this cluster were erratic and unsuitable for use.

The most probable explanation for the void encountered at Piezometer C-2 is that the drilling encountered a cave or incipient sinkhole. The

bedrock under AAAP is limestone which has the potential to develop karst features. The appearance of sink holes has been confirmed in the Childersburg area. A cavern, Onyx Cave, is open to the public and is located within 10 kilometers of AAAP.

#### 2.4.3 SLUG TESTS

Use of the electronic instruments for the precise measurement of water levels was generally very successful. The problems arising were mostly mechanical in nature.

The 3.5-inch by 8-foot mechanical slug was selected to give the maximum possible water displacement in the 4-inch-diameter wells. However, on several occasions, the tight fit between the slug and the casing (1.2 cm) caused the slug to become lodged because it did not allow for slight deflections in the casing or kinks in the sensor cable.

The water level in Well P-39 was low enough so that the bottom of the well contained only approximately 0.9 meter of water. This was not a sufficient quantity to allow testing by this procedure.

#### 3.0 LABORATORY ANALYSIS OF NITROAROMATIC COMPOUNDS

The procedures used to analyze the water samples collected from monitor wells for this phase were identical to those used in the Phase I study. The following sections are reproduced from that report.

The method used for analysis of nitroaromatic compounds in water was developed from the USATHAMA-supplied tentative gas chromatographic procedure for trinitrotoluene and related compounds in water. A modification of this method using three 2-ml extractions with toluene of a 250-ml water sample was employed for this survey. Three extractions with small amounts of toluene were used rather than extracting once with a larger volume of solvent followed by a solvent concentration step. Preliminary testing indicated that 2,4,6-trinitrotoluene and 1,3,5-trinitrobenzene extracted into methylene chloride were susceptible to thermal degradation during solvent concentration. Toluene was chosen as the extracting solvent because it is a good solvent for nitroaromatic compounds and because it is compatible with gas chromatographic electron-capture analysis (GC/EC). The single toluene extraction was satisfactory for all seven nitroaromatic compounds screened and quantitated using GC/EC. Six of the compounds (2,4-dinitrotoluene, 2,6-dinitrotoluene, trinitrotoluene, nitrobenzene, 1,3-dinitrobenzene, and 1,3,5-trinitrobenzene) were detected using one set of instrumental conditions. Tetryl detection required different conditions and a different column.

All groundwater extractions were performed on samples that had been filtered through 0.45-micrometer (um) membrane filters immediately after collection. Any emulsions that formed during extraction were broken by centrifuging the emulsified portions and drawing off the toluene layer.

### GC Analytical Conditions

Two different columns and sets of temperature regimes were required to detect all seven nitroaromatic compounds. Column conditions for analysis of the six selected nitrobenzene and nitrotoluene compounds consisted of a 6-foot by 2-mm inside diameter (i.d.) glass column packed with 3-percent OV-225 on 100/120-Mesh Gas Chrom Q. Tetryl was analyzed on a 3-foot by 2-mm i.d. glass column packed with 1.5-percent OV-17/1.95-percent QF-1 on 100/120-Mesh Gas

Chrom Q. The nitrotoluene/nitrobenzene analysis consisted of a 2-temperature ramp program performed on a Perkin-Elmer Sigma 2 Gas Chromatograph equipped with an electron-capture detector. The temperature program included isothermal hold at 100°C for elution of nitrobenzene, an isothermal hold at 165°C for elution of the dinitrotoluenes and dinitrobenzene, and a final temperature hold at 200°C for trinitrotoluene and trinitrobenzene. A temperature program at 15°C increase per minute was employed between each isothermal hold.

The gas chromatographic behavior of tetryl presented particular problems. Tetryl is sensitive to thermal decomposition on gas chromatographic columns. Because of this behavior, a temperature of 165°C was found to be the maximum allowable column temperature for detection of tetryl. New columns had to be silanized thoroughly by the injection of several 10-microliter (ul) volumes of silanizing agent (Silyl 8) before an acceptable peak shape was obtained for tetryl. Injection of several 5-ul volumes of a 1-ppm tetryl stock followed by several solvent injections also improved the chromatographic behavior of tetryl. Overall, GC/EC analysis was not an ideal method for tetryl analysis but did produce an acceptable linear response and sensitivity for use in this survey.

#### 4.0 TECHNICAL RESULTS

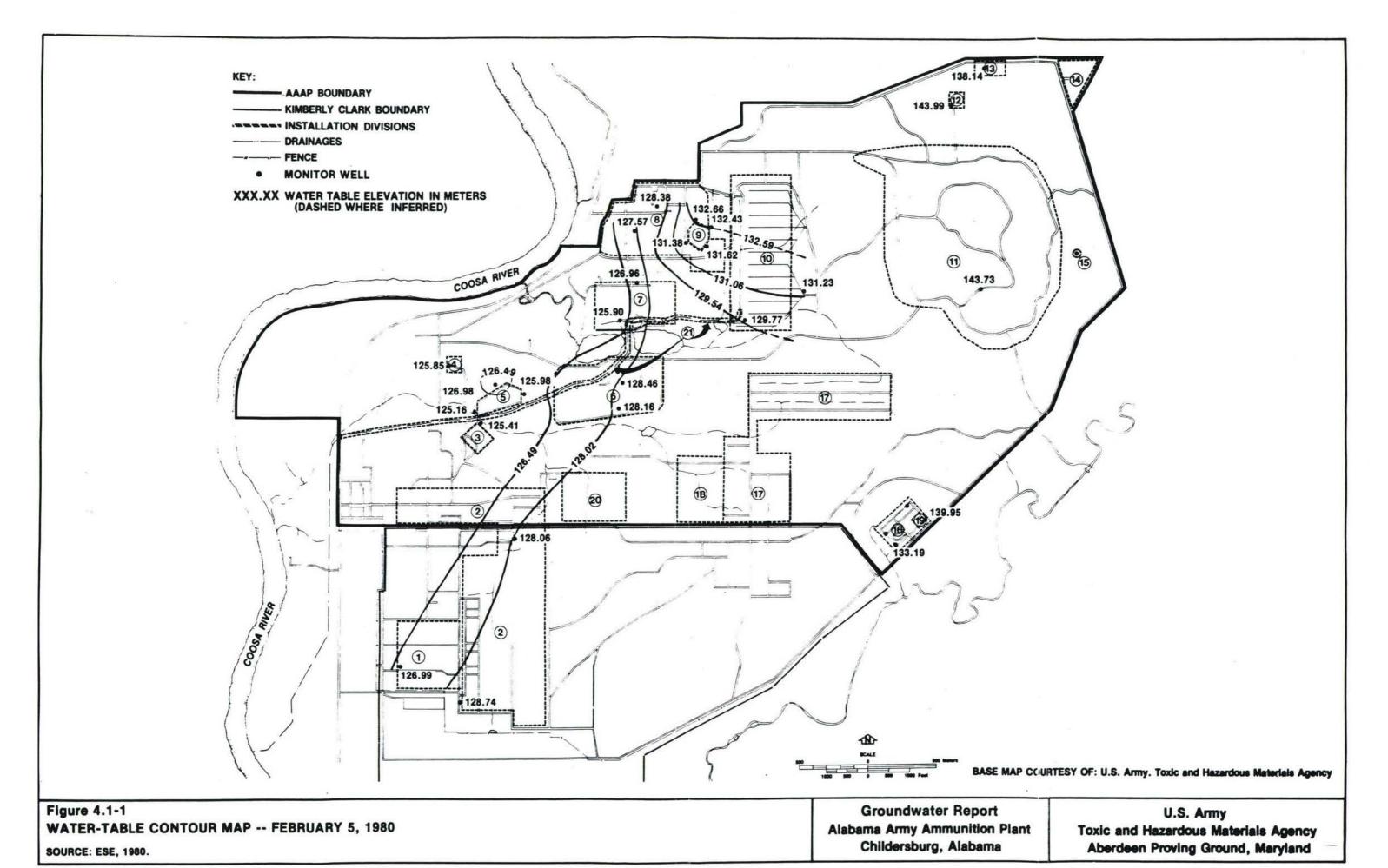
#### 4.1 GROUNDWATER HYDROLOGY

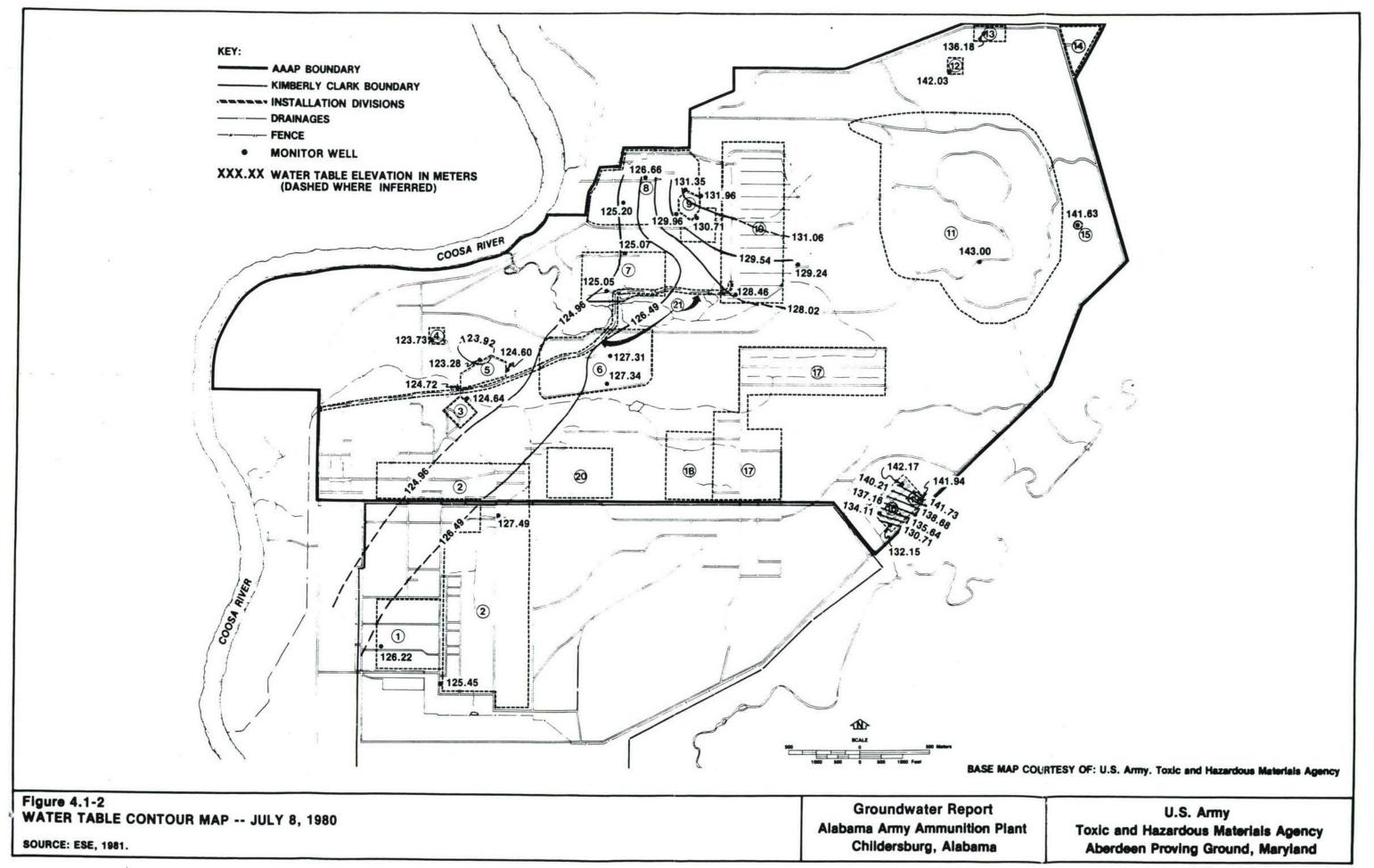
#### 4.1.1 WATER-TABLE AQUIFER

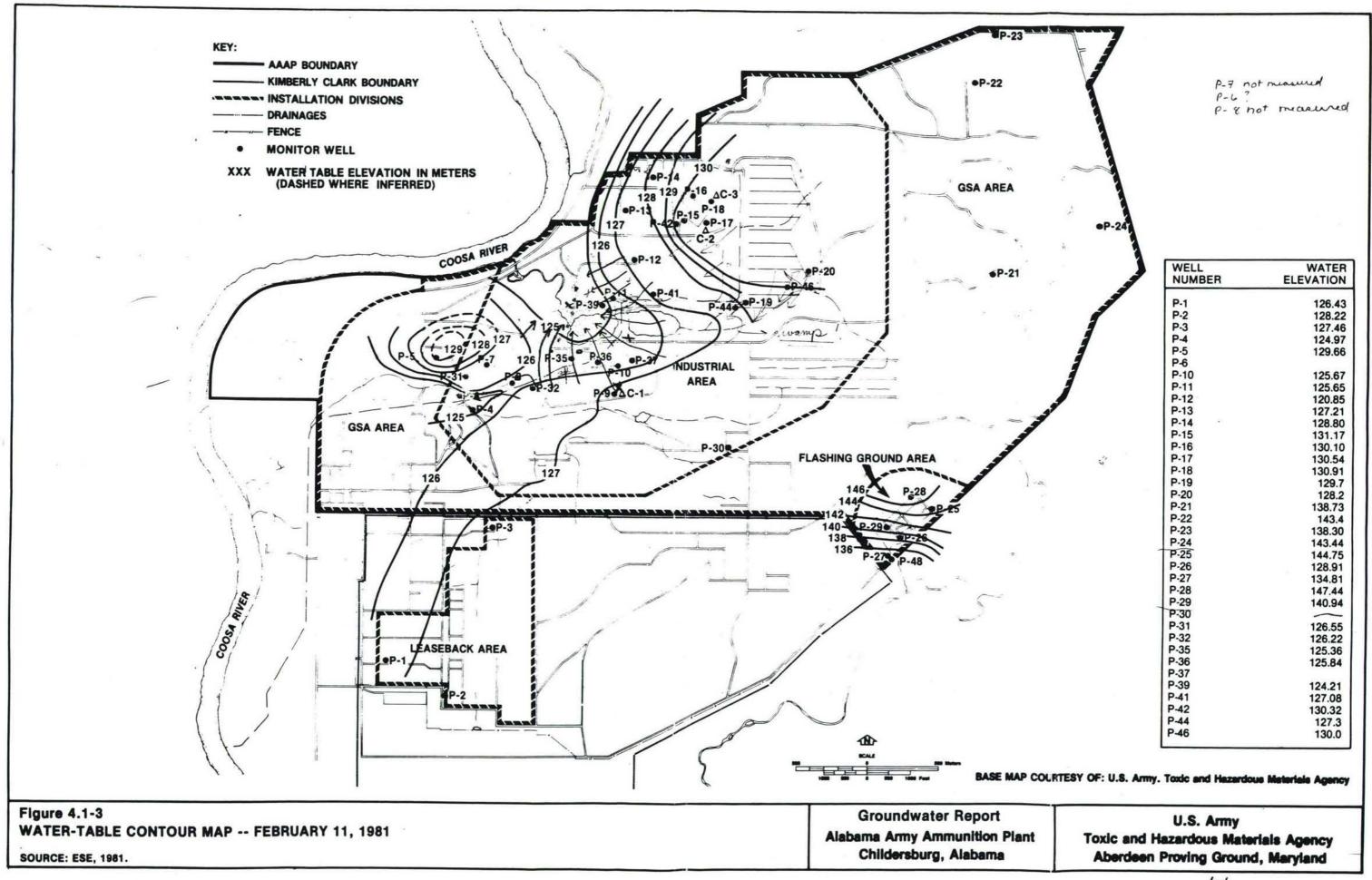
Three water-table maps were prepared from the water-level measurements at AAAP. Figures 4.1-1 and 4.1-2 show the water table on February 5, 1980, and July 8, 1980, during the winter and summer rainy seasons, respectively. After completion of the additional monitor wells, an additional set of water-level data was collected from all 38 monitor wells on February 11, 1981. The water-table map of these data is presented in Figure 4.1-3. The increased number of data points permitted a more precise definition of the water-table conditions, especially in the high-explosives manufacturing area near the Beaver Pond, Red-Water Ditch, and Crossover Ditch drainage systems.

Comparison of the three maps reveals a strong similarity of the shape of the water-table surface in all three situations. The highest land elevations in the eastern portions of the base have the highest water-table levels. The lowest land elevations, also the lowest water table, occur near the western part of the base near the Coosa River and southern base boundary near Talladega Creek. In the center, more level part of the base, the water-table gradient flattens considerably. In the center of the base, ground water in the water-table aquifer flows perpendicular to the contour lines toward the interior drainage system (Red-Water Ditch, Beaver Pond, and Crossover Ditch drainage systems). In the southern part of AAAP near the Flashing Ground, the water table dips steeply to the south and flows toward Talladega Creek.

The area near Wells P-5 and P-7 north of the Red-Water Storage Basin is a topographic divide between the Red-Water Ditch and Crossover Ditch drainage systems and the Coosa River. Apparently (at least seasonally),







a groundwater mound which drains to both the river and the ditch develops in this area. The July 8, 1980 water-table map, however, indicates that the water level of both Wells P-5 and P-7 was slightly below that of Wells P-6 and P-8. This water-level difference suggests the possibility of occasional groundwater movement north from the Red-Water Storage Basin toward the Coosa River and supports the conclusion in the previous report (ESE, 1981) that the contamination found in Well P-6 in February 1980 has migrated from contaminated sediments in the Red-Water Ditch. Analysis of samples taken from Well P-6 on February 25, 1981, did not show any quantifiable contaminants. On that date, the groundwater gradient was toward the Red-Water Ditch.

#### 4.1.2 CONTAMINATION MIGRATION POTENTIAL

The migration rate of contaminants in soil is directly related to the movement (both horizontal and vertical) of ground water. The factors involved in determining this movement are the hydraulic conductivity and porosity of the soils and the water-table slope.

### Horizontal Migration

To estimate the horizontal migration potential in the water-table aquifer, the hydraulic gradients were measured from the water-table maps. The horizontal permeability was measured by slug testing seven monitor wells. Porosity was estimated from published data (Walton, 1970).

The potential rate of horizontal pollutant movement can be estimated by using the following equation derived from Darcy's Law:

$$\overline{\mathbf{v}} = \frac{\mathbf{k}}{\mathbf{n}} \mathbf{I}$$

where:  $\overline{v}$  = Average linear velocity (cm/sec),

k = Hydraulic conductivity (cm/sec),

n = Porosity, and

I = Hydraulic gradient.

The average horizontal conductivity was calculated to be  $4.6 \times 10^{-5}$  cm/sec. This value appears to characterize the Explosives Manufacturing Areas and the Flashing Ground. In all cases, the porosity was assumed to be 0.5.

The Flashing Ground has the steepest gradient (0.0275) measured during this study. Applying this gradient to the above equation, a horizontal rate of movement of 7.9 meters per year may be expected. Calculations of this type assume that the soil is saturated at all times and that the gradient does not change. Since the drainage feature along the southwestern end of the Flashing Ground is often dry, as were three of the wells in February 1980, the two assumed conditions will result in a conservative estimate of migration rate; thus, the rate of movement is probably considerably less than the estimated 7.9 meters per year.

The high-explosives manufacturing area in the central part of AAAP has a much lower hydraulic gradient (near 0.010). This value was calculated by drawing several flow lines across the water-table contours and averaging the slopes. Using this value gives a potential horizontal rate of movement of 2.9 meters per year. Again, this value assumes a continuous supply of water available to flow with no seasonal change in gradient and, therefore, is a conservative estimate.

### Vertical Migration

The potential for vertical groundwater movement depends on the same variables (head, gradient, and hydraulic conductivity) described in the previous sections. The measurements used to determine these variables were taken from Piezometer Clusters C-1 and C-3.

Water-level measurements were taken at both clusters on January 22, 23, and 27, and February 11, 1981. During this 3-week period, four rainfall events occurred, each of which affected the shallow water table. The deep piezometers continued to show a steady rise, as expected, because winter is normally a period of recharge to the lower aquifer.

For these calculations, the hydraulic gradient (I) was assumed to be the elevation difference between the water level in Piezometer Clusters C-1 and C-3 divided by the elevation difference between the center of the two piezometer screens.

A summary of the water surface elevations and vertical gradients is presented in Table 4.1-1. On every date, there is a significant head difference between the water-level elevation of the shallow and deep piezometers. For this study, the data from the middle piezometer were used as supporting data to check the linearity of the gradients. The hydraulic gradients developed between C-1A and C-1B remained fairly uniform (0.28 to 0.46) throughout the period, while gradients between C-3A and C-3B normally were 0.20 to 0.27 (except after the heavy rainfall of February 10 the value increased to 0.77, due largely to the lower permeability/denser compaction of soil at that site as indicated by the higher standard penetration blow counts). These hydraulic gradients are significant and indicate a high probability of some vertical pollutant migration.

Applying the following formula (from Darcy's Law), the quantity of water moving vertically can be calculated.

Q = kIA

where: Q = Discharge (cm<sup>3</sup>/sec),
k = Hydraulic conductivity (cm/sec),
I = Hydraulic gradient, and

 $A = Area (cm^2).$ 

Table 4.1-1. Summary of Water Surface Elevations and Vertical Gradients

		January 22, 1981	22, 1981	January 23, 1981	23, 1981	January 27, 1981	1861 , 13	February 11, 1981	11, 1981
Piezmeter	Screen Elevation	Water Surface Elevation	Gradient	Water Surface Elevation	Gradient	Water Surface Elevation	Gradient	Water Surface Elevation	Gradient
Cluster 1			.73/. =.12	51.2			1		
Shallow (B) Gradient Between	124.84	126.66	5, 0.12	126.71	0.11	126.70	0.10	128.54	0.36
B and C Middle (C) Gradient Between	118.73	125.93	0.00	126.02	0.83	126.10	0.58	126.36	0.19
C and A Deep (A)	114.08	121.74		122.16		123.42		125.45	
Gradient Between A and B			97.0		0.42		0.31		0.28
Cluster 2									
Shallow (B) Gradient Between	126.06	126.97	-0.01	126.93	-0.02	126.85	0.05	131.94	0.59
B and C Middle (C) Gradient Between	123.51	127.00	0.44	126.99	0.32	126.89	0.32	130.42	0.88
C and A Deep (A)	119.17	125.09		125.19		125.50		126.62	
Gradient Between A and B			0.27		0.25		0.20		0.77

Note: All elevations are given in meters above mean sea level.

Source: ESE, 1981.

Assuming that the vertical permeability reported by Keeler (1980) is typical of this soil type  $(1 \times 10^{-6} \text{ cm/sec})$  with hydraulic gradient of 0.37, a 1-meter-square section of soil would conduct water to the lower aquifer at a rate of 95 liters per year per square meter (equivalent to 9.5 cm rainfall per year to the limestone aquifer). This equates to an average vertical velocity of 0.23 meter per year.

### 4.2 GROUNDWATER QUALITY

Water quality and the contamination status of the water-table aquifer in the Industrial Area, including the Flashing Ground, are described in this section. Samples were collected on February 25, 1981, from each of the seven wells in which contamination had been observed during the Phase I survey (ESE, 1981) and from the 11 additional wells constructed during Phase II. An additional sample was collected from Well P-23 to serve as a background control since this well did not contain detectable contamination during the Phase I survey. Samples were collected as described in Section 2.2 and couriered to the ESE laboratory for chemical analysis. Specific conductance and pH were measured on site, prior to filtration. Samples were chilled and protected from light at all times to minimize changes in their constituents. All 19 samples were analyzed for the following nitroaromatic compounds: nitrobenzene, 2,4-dinitrotoluene, 2,6-dinitrotoluene, 1,3-dinitrobenzene, 1,3,5-trinitrobenzene, 2,4,6-trinitrotoluene, and tetryl.

The most important groundwater quality results are summarized in the following paragraphs. These Phase II results are compared to the results of the Phase I survey (ESE, 1981) to describe the contamination status of the water-table aquifer underlying the explosives manufacturing areas [the Southern and Northern TNT Manufacturing Areas (Study Areas 6 and 7) and the Tetryl Manufacturing Area (Study Area 10)], the southern portion of the Acid/Organic Manufacturing Area (Study Area 8), the liquid-waste storage areas [the Red-Water Storage Basin (Study Area 5) and the Aniline Sludge Basin (Study Area 9)], the Red-Water Ditch (Study Area 21), and the Flashing Ground (Study Area 16). As

identified in the Phase I report (ESE, 1981), the soil and/or aquatic sediments of all these study areas are contaminated to some degree by nitroaromatic residues. The locations of the monitoring wells are shown in Figure 4.2-1.

The complete groundwater quality data base has been entered in the USATHAMA Chemical Data Files in the UNIVAC 1108 at Aberdeen Proving Ground, Maryland. The Phase I groundwater quality data are contained in Tier-2 file ALSBCGW81142. The Phase II data are contained in Tier-2 file ALSBCGW81160.

#### 4.2.1 SPECIFIC CONDUCTANCE AND pH

The results of the specific conductance measurements made during the Phase I survey suggested that dissolved salts had affected the characteristics of the water-table aquifer under the Industrial Area. The specific conductance of samples from wells outside this area ranged from 58 to 180 umho/cm; within the Industrial Area, the conductance ranged from 76 to 552 umho/cm. During the Phase II survey, specific conductances were lower than during Phase I. The results of the pH and specific conductance measurements are presented in Table 4.2-1. The Phase I data are included for comparison.

Except for Wells P-6 and P-26, conductivities at all of the wells sampled during both phases were observed to be a factor of 2 to 3 lower in February 1981 compared to February 1980. Wells P-6 and P-26 were lower by a factor of 4. The rainfall which occurred the month preceding sampling was above normal for both years; however, January 1981 was wetter than January 1980 (7.72 cm above normal and 5.64 cm above normal, respectively). Secondly, more than twice as much rainfall fell in the 15 days preceding the Phase II sampling. A total of 16.58 cm fell during this period, including major storm events which brought 9.14 cm of rain on February 10, 1981, and 4.72 cm on February 17, 1981. For the Phase I survey, total rainfall during the 15 days prior to sampling was only 6.68 cm. These data are from NOAA (1980, 1981) records collected at the Childersburg, Alabama Water Treatment Plant. Dilution of the

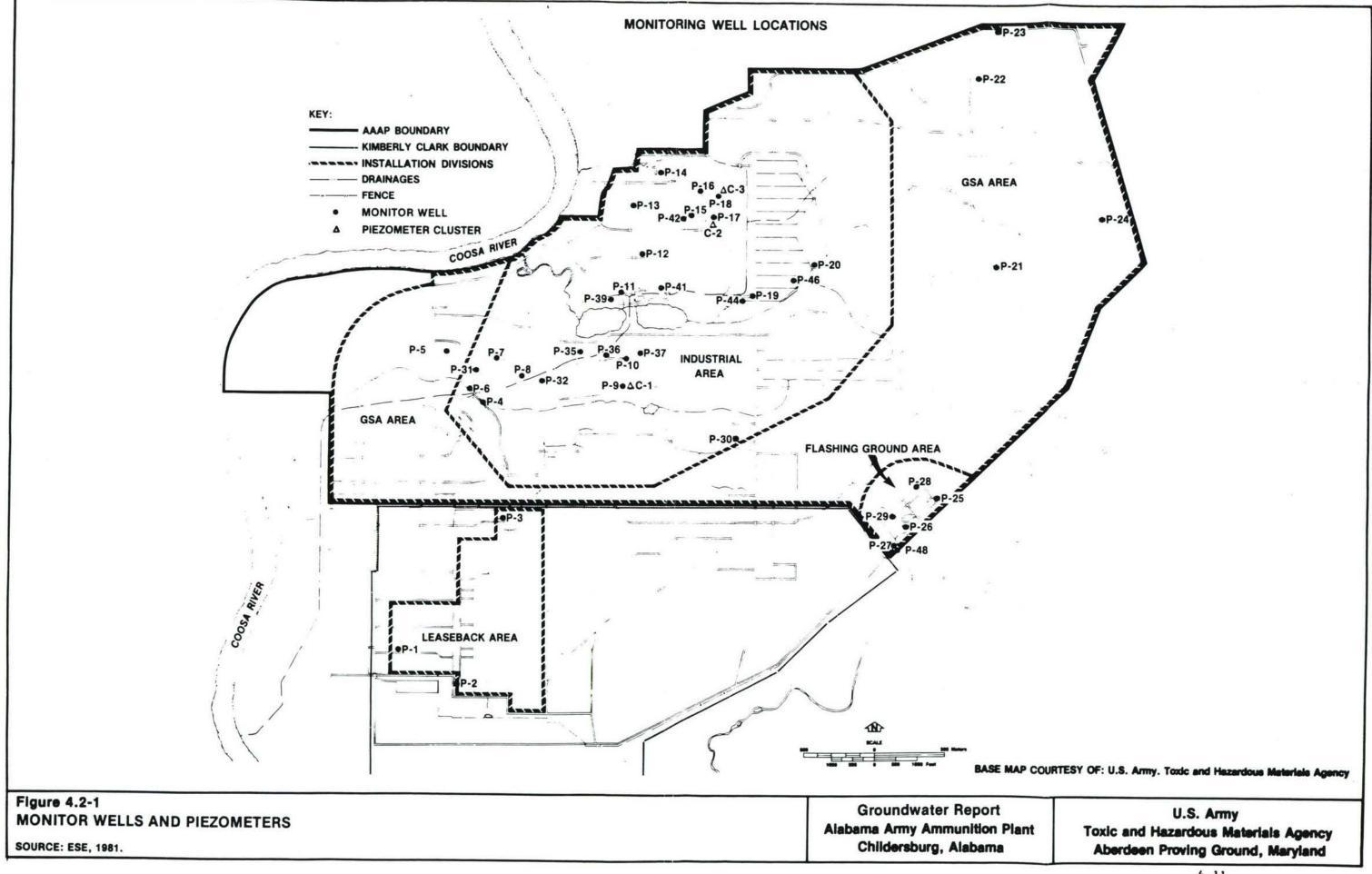


Table 4.2-1. Comparison of pH and Specific Conductance in the Water-Table Aquifer--February 1980 and February 1981

	Loca	tion	February	1980†	February	1981†
			Specific		Specific	
Well	Study	AAAP	Conductance	pН	Conductance	pH
Number	Area	Area*	(umho/cm)	Units	(umho/cm)	Units
P-1	1	LBA	180	6.1		
P-2	1 2 2	LBA	74	5.9		
P-3	2	LBA	768	6.7		
P-4	3	IND	33	6.1		
P-5	4	IND	282	6.3		
P-6	5,21**	IND	150	6.4	35	6.1
P-7	5	IND	76	6.0		
P-8	5,21**	IND	384	6.7		
P-9	6	IND	492	8.2		
P-10	6 7 7	IND	354	5.4	122	6.2
P-11	7	IND	382	6.8	190	6.5
P-12	7	IND	232	6.2		
P-13	8	IND	552	6.5		
P-14	8	IND	186	6.2		
P-15	8,9**	IND	122	6.0	76	6.2
P-16	8,9**	IND	40	5.8		
P-17	8,9**	IND	389	6.3		
P-18	8,9**	IND	195	6.1		
P-19	10	IND	236	6.2	76	6.0
P-20	10	IND	50	5.6	19	5.7
P-31	5**	IND			87	5.9
P-32	5,6**	IND			95	5.6
P-35	6	IND			169	6.0
P-36	6	IND			43	5.0
P-37	6 7	IND			272	6.1
P-39	7	IND			158	5.5
P-41	7	IND			158	6.0
P-42	8,9	IND			87	5.7
P-44	10**	IND			144	3.4
P-46	10	IND	-		98	5.6

Table 4.2-1. Comparison of pH and Specific Conductance in the Water-Table Aquifer--February 1980 and February 1981 (Continued, Page 2 of 2)

	Loca	tion	February	1980†	February 1	1981†
Well Number	Study Area	AAAP Area*	Specific Conductance (umho/cm)	pH Units	Specific Conductance (umho/cm)	pH Units
P-21	11	GSA	77	6.0		
P-22	12	GSA	120	6.2		
P-23	13	GSA	93	6.0	33	6.0
P-25	16	IND	58	5.9		
P-26	16	IND	133	6.0	30	5.5
P-48	16**	IND			104	6.3

<sup>\*</sup> AAAP Area: GSA = General Services Administration Area

LBA = Leaseback Area

IND = Industrial Area (Explosives Manufacturing, Flashing Ground, Manhattan Project Area, Sanitary Landfill)

Source: ESE, 1980 and 1981.

<sup>†</sup> Sampled February 6, 1980, and February 25, 1981.

<sup>\*\*</sup>Well is not located within study area.

water-table aquifer immediately prior to the Phase II sampling probably accounts for the lower specific conductances observed. The monitor wells are constructed with a filter pack surrounding the well screen, extending from near the average water-table elevation to the bottom of the well. During bailing and sampling activities, this filter pack acts as a vertical conduit to conduct the lower-conductance shallow ground water downward to the well screen to mix with water entering from other parts of the aquifer. The resulting sample is a vertical composite from all levels of the aquifer including water from above the contaminated zone. In spite of the overall lower conductivities observed, the ground water sampled in the central part of the Industrial Area was higher in conductivity than the ground water at the edge of the Industrial Area. High conductivity also was related to detection of nitroaromatic residues. This pattern is similar to that observed during Phase I sampling.

With the exception of Well P-44, the pH values observed during Phase II were similar to those observed during Phase I. A pH value of 3.4 was observed during Phase II at Well P-44. This value is lower than any other observed in the environmental survey, including 1980 and 1981 values for Wells P-19 and P-20 and 1981 values for Well P-46 located nearby. Well P-44 had the highest observed conductivity of these wells during the Phase II sampling, however. The source of acidity at this well location cannot be confirmed or identified by other data.

#### 4.2.2 NITROAROMATIC RESIDUES

Table 4.2-2 presents the results of analysis of the trinitrotoluenerelated nitroaromatic compounds and tetryl in the 18 wells sampled
during Phase II. Phase I data for Wells P-6, P-10, P-11, P-15, P-19,
P-20, and P-26 are included for comparison. The Phase II results
confirmed the presence of nitroaromatic residues in the ground water
underlying the Northern and Southern TNT Manufacturing Areas.
Comparison of the 1980 and 1981 results from Wells P-10 and P-11
suggests that the dilution effect described in the preceding paragraphs

Table 4.2-2. Comparison of the Concentration of Nitroaromatic Residues in the Water-Table Aquifer—February 1980 and February 1981

H	2,4 rinitr	2,4,6- Trinitrotoluene	2,4- Dinitroto	4- toluene	2, Dinitro	2,6- Dinitrotoluene	Nitrob	enzene	1, Dinitro	1,3- Dinitrobenzene	1,3 Trinitr	1,3,5- Trinitrobenzene	Tet	Tetrvl
	1980	1981	1980 1981	1981	1980	1981	1861 0861	1981	1980	1981	1980	1981	1980	1981
	0.41	4.15	1.0	3.01	1.3	3.8	65.8	<b>(</b> 1)	41.8	8.45	6.3	69.7	3.2	(23.9
		4.1>		3.0	#	3.81		<b>(1)</b>		4.81		<9.7		(23.9
		41.41		3.0		3.8		<b>(1)</b>		8.4>		(9.7		<b>43.9</b>
10	10,270	4,540	4,340	1,620	98	20%	36.1	<170	997	<48.2	4,380	2,010	3.2	(23.9
		47.6		3.0		3.81		<b>(1)</b>		4.8	9	49.7		<23.9
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		<1.4		3.0		3.81		<b>(1)</b>		8.45		49.7		<23.9

Source: ESE, 1980 and 1981.

<sup>\*</sup> Sampled February 6, 1980, and February 25, 1981.
† Trace amounts observed below the quantitative detection limit.

also lowered the concentrations of nitroaromatic residues in the ground water sampled in 1981 (Phase II).

The quantifiable detection limits attained during the 1981 survey were slightly higher than for the 1980 results. Detection limits for each set of analyses were determined in accordance with the Quality Control Plan. These limits are determined statistically from regression analysis of uncontaminated water from the AAAP site which was spiked with known concentrations of each analyte. Because of this procedure analytical detection limits vary slightly among analytical sets. The detection limits for the dinitrotoluene isomers and the nitrobenzene compounds were high on several samples which contained high levels of 2,4,6-trinitrotoluene (TNT). In Well P-10, sampled during 1981, the high level of TNT made it impossible to analyze the sample without making a ten-fold dilution of the extract. The chromatographic column would have been destroyed at a higher concentration level. detection limit for nitrobenzene and 1,3-dinitrobenzene was therefore 10 times higher than for samples in which the extract could be analyzed without dilution. A similar situation raised the dilution limit for 2.6-dinitrotoluene in the 1981 sample from Well P-11, although other nitroaromatic residues could be quantitated without dilution. In this sample, the TNT peak interfered only with the 2,6-dinitrotoluene.

As shown in Table 4.2-2, chromatographic peaks suggestive of the presence of traces of the analytes, but below quantitative detection levels, were frequently observed. Considering the differences in detection limits and dilution, the 1980 and 1981 data on the Phase I wells are comparable. Considered together, the 1980 and 1981 data on the Phase I and Phase II wells suggest the following pattern of contamination in the water-table aquifer at AAAP.

Overall, the major sources of groundwater contamination appear to be located around the former Washer-Flaker House areas in both the Southern and Northern TNT Manufacturing Areas. The Southern TNT Manufacturing

Area (Study Area 6) has the highest level of contamination (Wells P-10 and P-37). Ground water from Well P-36, located adjacent to TNT Line G, contained no detectable nitroaromatic residues, and water at Well P-35 contained significantly lower concentrations than the samples from Wells P-10 and P-37. These results suggest that the pattern of contaminated ground water in the TNT Manufacturing Areas consists of pockets of heavily contaminated water migrating from discrete sources rather than including large areas. In the Northern TNT Manufacturing Area (Study Area 7), the level of contamination was lower (see Wells P-11, P-39, and P-41).

Small amounts of nitroaromatic residues appear to be contaminating the ground water near the Red-Water Storage Basin and lower Red-Water Ditch, as shown in Table 4.2-2. Trinitrotoluene and 2,4- and 2,6-dinitrotoluene were observed at concentrations near the detection limit during the Phase I sampling program. No quantifiable levels were found during the 1981 sampling program. During drilling of Well P-31, a strong nitroaromatic odor was observed. No detectable nitroaromatic compounds were observed in sampling of this well; however, chromatographic peaks were observed at levels far below detection limits in water. Certain of the nitroaromatics such as nitrobenzene and the dinitrotoluenes are volatile, have a particularly strong odor, and can be detected by the sense of smell at extremely low concentrations in air. In augering the hole, the soil was likely heated and sufficient material volatilized to detect by olfaction, yet the concentration in the ground water was below chemical detection limits. Both 2,4- and 2,6-dinitrotoluene, as well as 1,3-dinitrobenzene, chromatographic peaks were observed in the sample from Well P-31; however, the concentrations were below the quantifiable limit. A non-quantifiable peak suggesting 2,4-dinitrotoluene was observed in a sample taken from Well P-6 during the 1981 sampling. No detectable nitroaromatic residues were observed in 1980 samples from Wells P-7 and P-8. The sample from Well P-32 contained less than quantifiable amounts of trinitrotoluene.

During Phase I, low concentrations of nitroaromatic residues were found in the ground water from Well P-15, downgradient from the Aniline Sludge Basin (Study Area 9). During Phase II, 2,4- and 2,6-dinitrotoluene were found in a sample of this ground water; however, concentrations were below the quantifiable limit. No contamination was observed in the aquifer at Well P-42, located just downgradient from Well P-15.

Tetryl, observed in the ground water at Well P-20 during Phase I, was not confirmed during the 1981 survey. Chromatographic peaks identifiable as trinitrotoluene, both dinitrotoluene isomers, and trinitrobenzene were observed in samples from Well P-44; however, these were below the quantitative detection limit.

During the Phase I survey, 3.6 ug/1 of 2,4-dinitrotoluene was observed in the ground water at the southern end of the Flashing Ground (Study Area 16). This contamination was not present during the 1981 survey. No quantifiable concentrations of nitroaromatic residues were found in samples from Well P-26 or Well P-48 located downgradient from the Flashing Ground. Trace quantities of materials identifiable as trinitrotoluene and dinitrotoluenes were observed in these wells; however, the concentrations were below the quantifiable detection limit.

#### 4.2.3 GROUNDWATER CONTAMINATION STATUS

The groundwater quality data from the Phase I and Phase II surveys indicate that the water-table aquifer underlying the Industrial Area at AAAP contains pockets of nitroaromatic contamination which appear to be localized near discrete sources of contamination related to the sites of previous industrial activity.

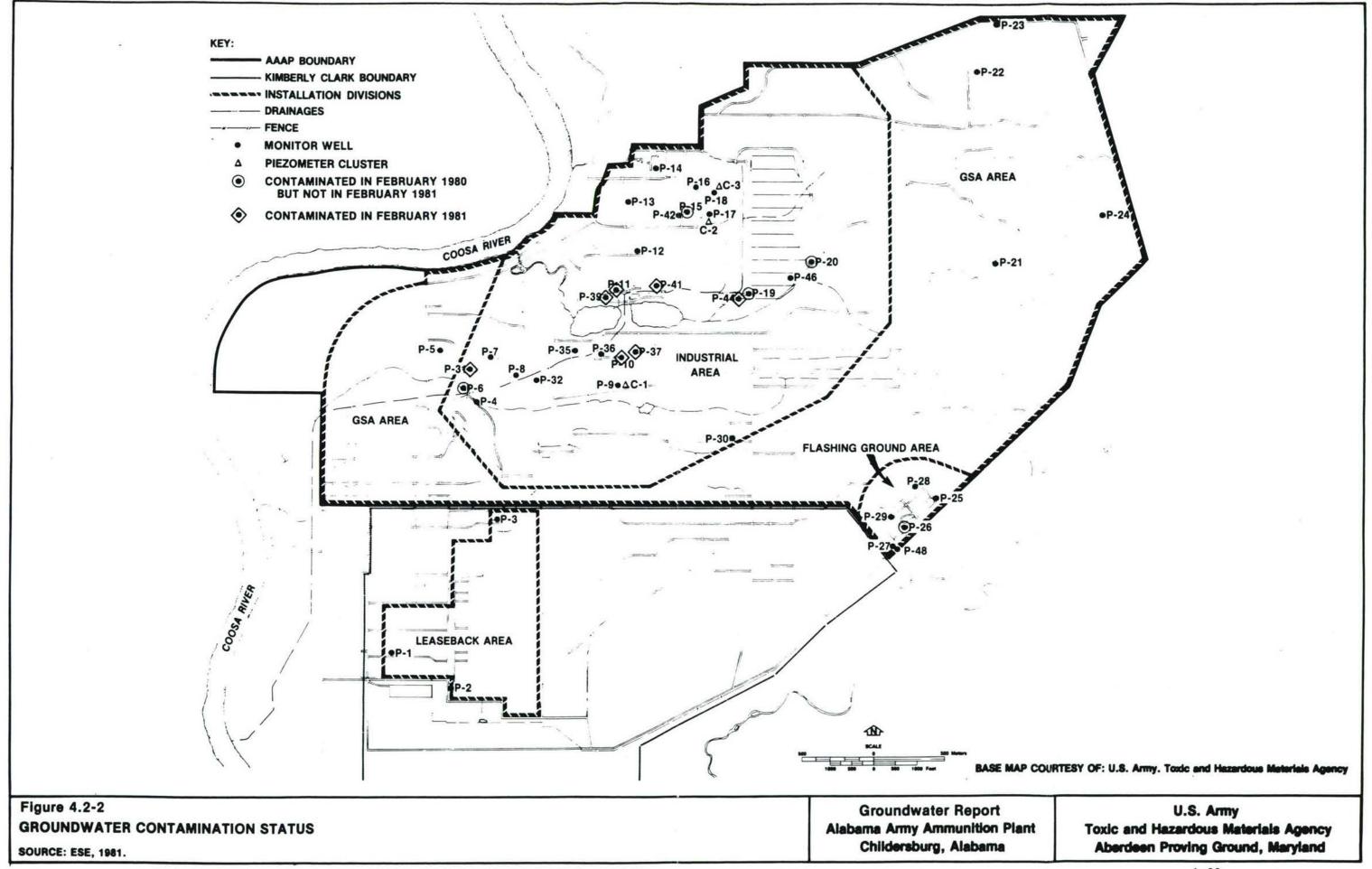
Concentrations of nitroaromatic residues just above the detection limit were observed at one well adjacent to the Red-Water Storage Basin and lower Red-Water Ditch. During Phase II, concentrations were below the detection limit at this well and at two other wells (Well P-31 located

adjacent to the Red-Water Storage Basin and Well P-32 located along the Red-Water Ditch). Apparently only small amounts of nitroaromatic residues are migrating from the contaminated sediments of these two water bodies. The presence of tetryl in Well P-20 was not confirmed during the Phase II survey; however, tetryl was observed in the sample from Well P-44.

The horizontal migration of contamination from the two TNT manufacturing areas has apparently been largely confined within the Industrial Area (Figure 4.2-2). This conclusion is based on the following evidence:

- The absence of detectable concentrations of nitroaromatic residues in samples from Wells P-4, P-5, P-7, P-8, P-9, P-12, P-13, P-16, and P-17 during the Phase I survey and in samples from Wells P-19, P-20, and P-42 during the Phase II survey.
- The presence of only non-quantifiable traces of nitroaromatic residues during the Phase II survey at Wells P-6, P-15, P-31, P-32, P-44, and P-46.

At the Flashing Ground, nitroaromatic contamination was below quantifiable limits during the Phase II survey. Only small amounts of contaminants (below detection limits) are moving horizontally downgradient at this location as leachate from the contaminated soil. There was sufficient rainfall immediately preceding the Phase II sampling to reduce contaminant levels below detection limits.



#### 5.0 CONCLUSIONS

The results of geohydrological and water quality studies of the water-table aquifer underlying the Industrial Area and the Flashing Ground at AAAP are presented in the preceding sections of this report. These data were gathered during Phase I, the Environmental Survey (ESE 1981), and Phase II, the groundwater contamination study. This section summarizes the important conclusions regarding the contamination status and contaminant migration potential in the water-table aquifer at AAAP.

The following conclusions can be made regarding the geohydrological characteristics of the water-table aquifer:

Water-level measurements taken in monitor wells for both Phase
I and Phase II indicate a strong similarity. The general flow
direction in the Industrial Area is toward the Coosa River and
the Red-Water Ditch, with a horizontal gradient of near
0.01 meter per meter.

At the Flashing Ground (Study Area 16), the water table slopes steeply to the southeast toward Talladega Creek at a gradient of 0.0275 meter per meter.

- 2. Horizontal migration rates were calculated using data collected from 13 slug tests conducted in monitor wells. These tests indicate that the ground water is moving downgradient at a rate of approximately 2.9 meters per year in the Industrial Area and 7.9 meters per year at the Flashing Ground (Study Area 16).
- Estimates of vertical leakance of water to the lower aquifer, based on hydraulic heads measured in two piezometer clusters, show that recharge occurs at a rate of approximately 95 liters

per year per square meter. This is equivalent to vertical rate of water movement in the Industrial Area of 0.23 meter per year.

The following conclusions can be made regarding the contamination status of the water-table aquifer:

- The Phase I survey (ESE, 1981) indicated that groundwater contamination was confined to the Industrial Area and the Flashing Ground (Study Area 16). The water-table aquifer underlying the Leaseback Area and the GSA Area is free from contamination.
- 2. The groundwater quality data from the Phase I and Phase II surveys indicate that the water-table aquifer underlying the Industrial Area at AAAP contains pockets of nitroaromatic contamination which appear to be localized near discrete sources of soil contamination primarily related to sites of previous industrial activity (Washer-Flaker Houses) within the Southern and Northern TNT Manufacturing Areas (Study Areas 6 and 7), and to spoil banks of contaminated Red-Water Ditch sediments within Study Area 6.
- 3. Based on the results of the Phase I and Phase II surveys, only small quantities of nitroaromatic residues appear to be migrating from contaminated sediments of the Red-Water Storage Basin, Red-Water Ditch, and Aniline Sludge Basin. This conclusion is based on observation of contaminant concentrations near the detection limit or below the quantifiable detection limit in wells located downgradient from these sources.
- 4. Increased specific conductance above the values observed in other areas at AAAP was observed in the wells within the Industrial Area. This observation was related to detection of nitroaromatic residues. A dilution effect was observed during the Phase II survey and was a result of antecedent rainfall conditions.

5. Nitroaromatic concentrations were diluted during Phase II as a result of antecedent rainfall conditions as indicated by the comparative Phase I and Phase II data. The major contaminants found during both surveys were 2,4,6-trinitrotoluene; 2,4- and 2,6-dinitrotoluene; 1,3-dinitrobenzene; and 1,3,5-trinitrobenzene.

During Phase I (ESE, 1981), several other nitroaromatic compounds, transformation products of 1NT, were identified in the sample from the most heavily contaminated well. These were 4-amino-2,6-dinitrotoluene; 3,5-dinitroaniline; 2-amino-4,6-dinitrotoluene; 2,4-dinitrophenol; and 2-methyl-4,6-dinitrophenol.

The horizontal migration of contamination from the two TNT manufacturing areas has apparently been largely confined within the Industrial Area. This conclusion is based on the following evidence:

- The absence of detectable concentrations of nitroaromatic residues in Wells P-4, P-5, P-7, P-8, P-9, P-12, P-13, P-16, and P-17 during the Phase I survey and in Wells P-19, P-20, and P-42 during the Phase II survey.
- The presence of only non-quantifiable traces of nitroaromatic residues during the Phase II survey at Wells P-6, P-15, P-31, P-32, P-44, and P-46.

In the Industrial Area, the closest horizontal downgradient distance from a contaminated well (P-11) to the AAAP boundary is approximately 670 meters. Using the calculated horizontal flow rate of 2.9 meters per year, the time required for contaminated ground water to move off site in the northwest direction is approximately 230 years.

The Flashing Ground is much closer to the boundary. Because of this proximity and the steeper groundwater gradient, the time required for

ground water to migrate the 25-meter distance to the boundary is approximately 3 years.

Based on the observations and measurements made in the two piezometer clusters, a calculation of time required for ground water to move vertically from the water-table aquifer to the lower limestone aquifer at Wells P-11 and P-10 shows time rates of 10 years and 33 years, respectively.

#### 6.0 REFERENCES

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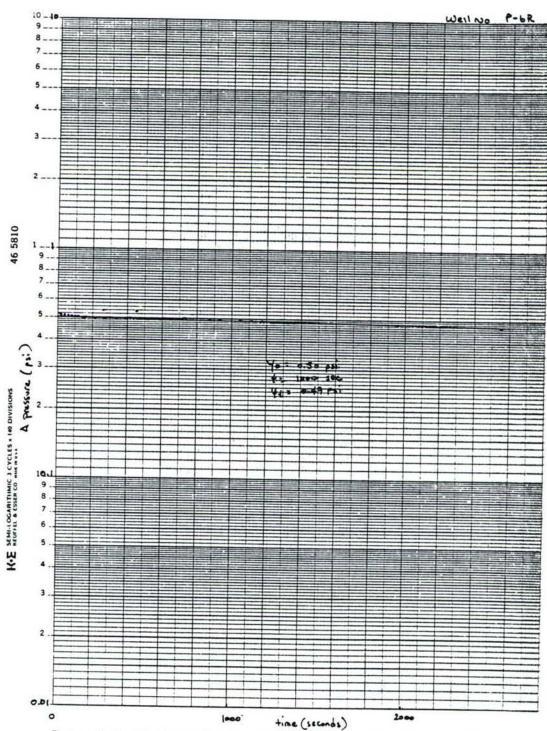
APPENDIX A
SLUG TEST CALCULATIONS

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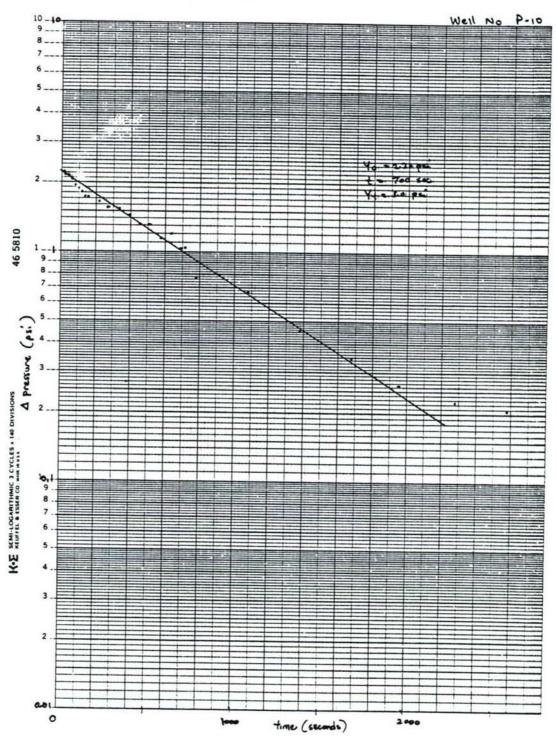
Data plot of elapsed time against change in pressure for Well P-6 (SI phase)

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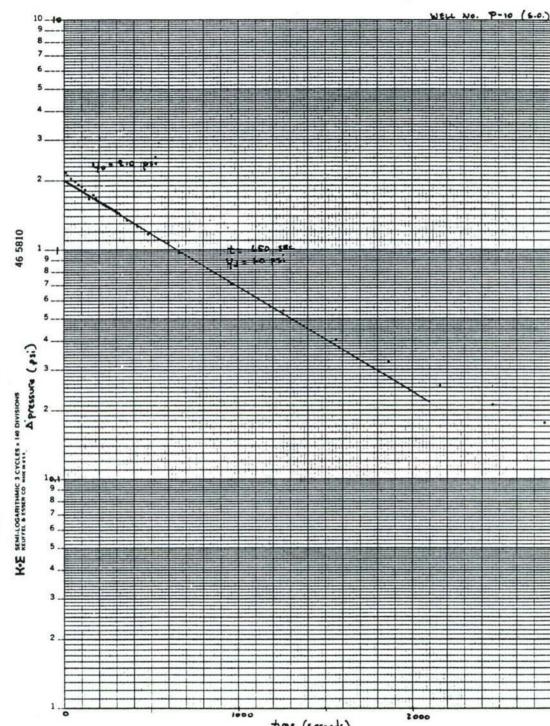
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Data plot of elapsed time against change in pressure for Well No. P-10 (SI phase)



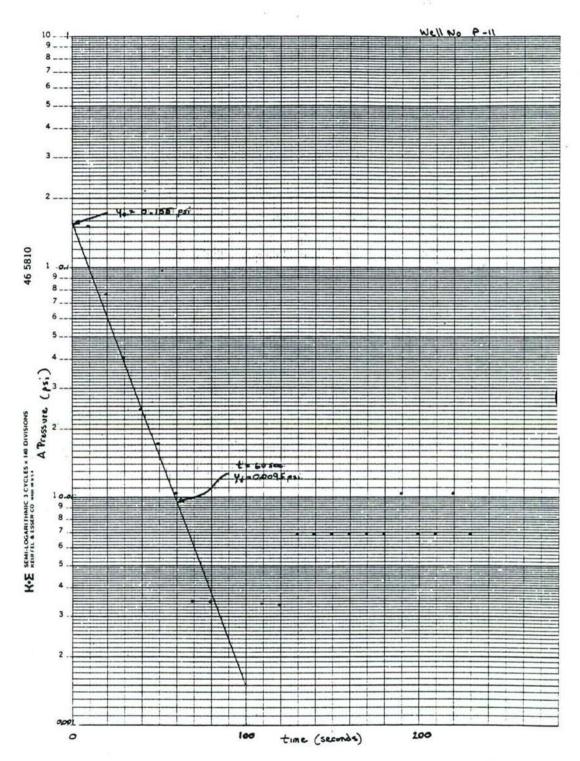
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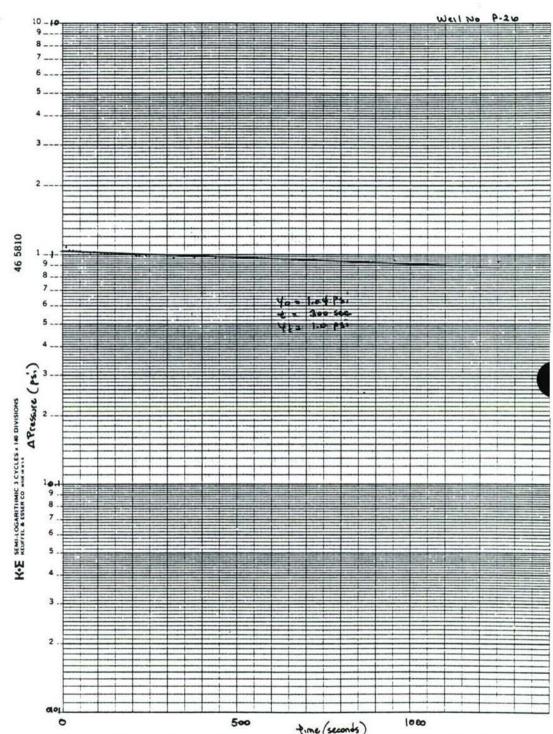
Data plot of elapsed time against change in pressure for Well No. P-11 (SI phase)

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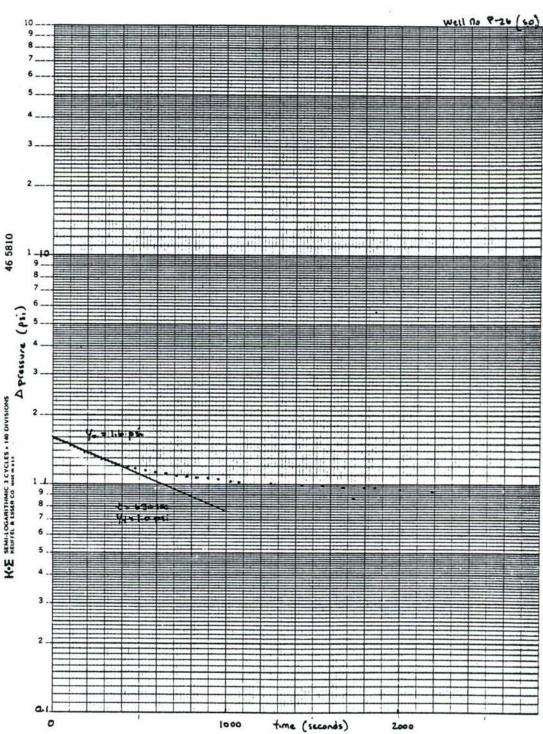
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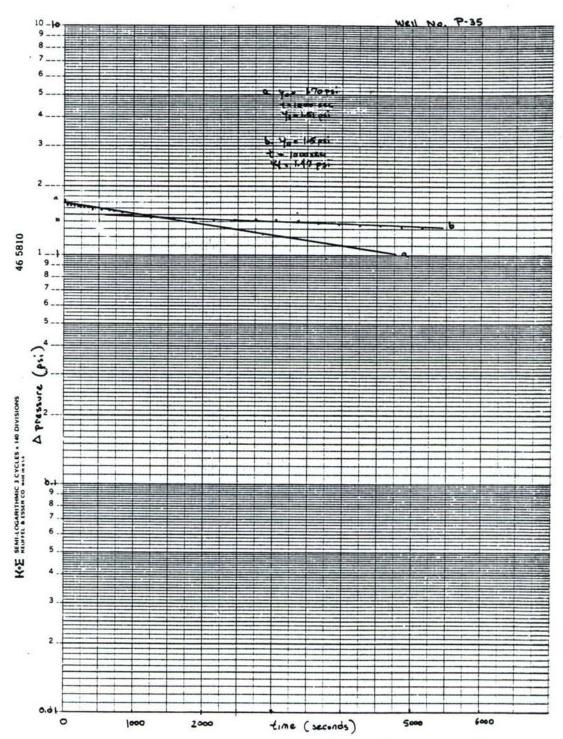
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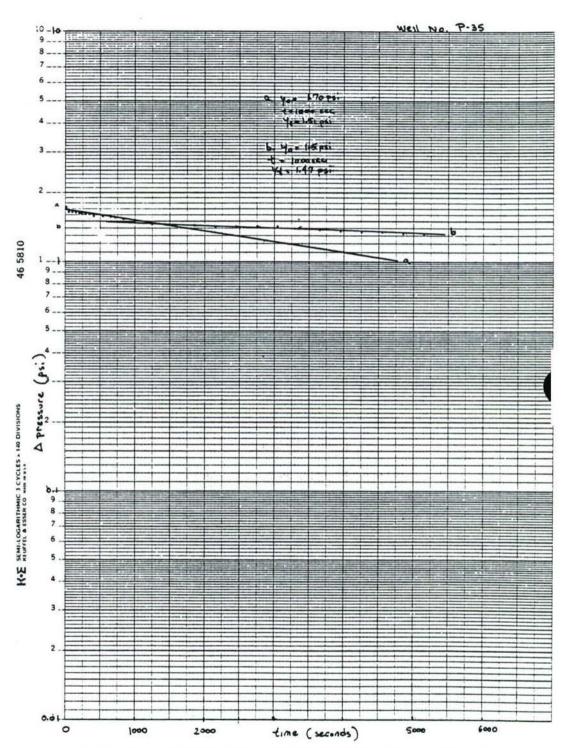
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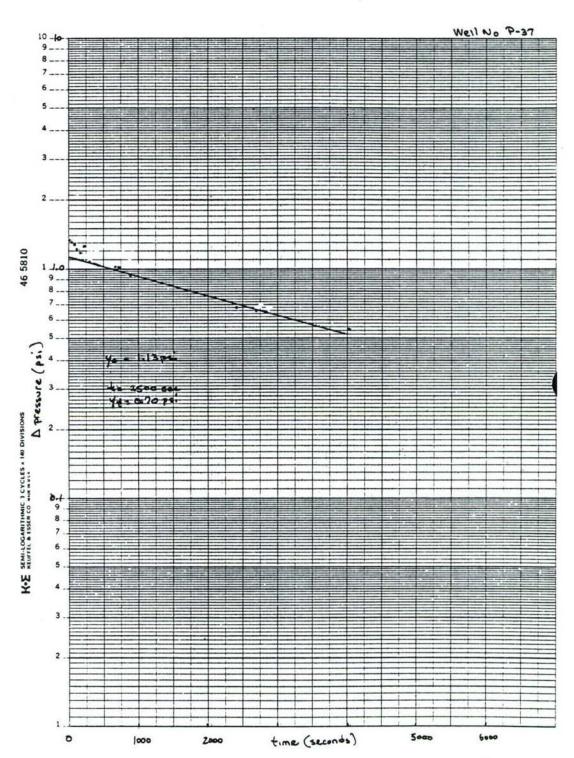


Data plot of elapsed time against change in pressure for Well P-35 (SO phase)

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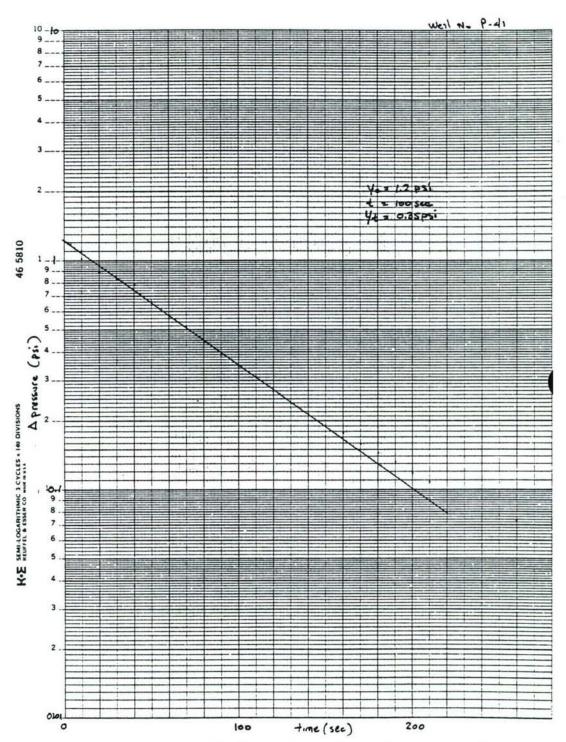
Data plot of elapsed time against change in pressure for Well No. P-37 (SI phase)

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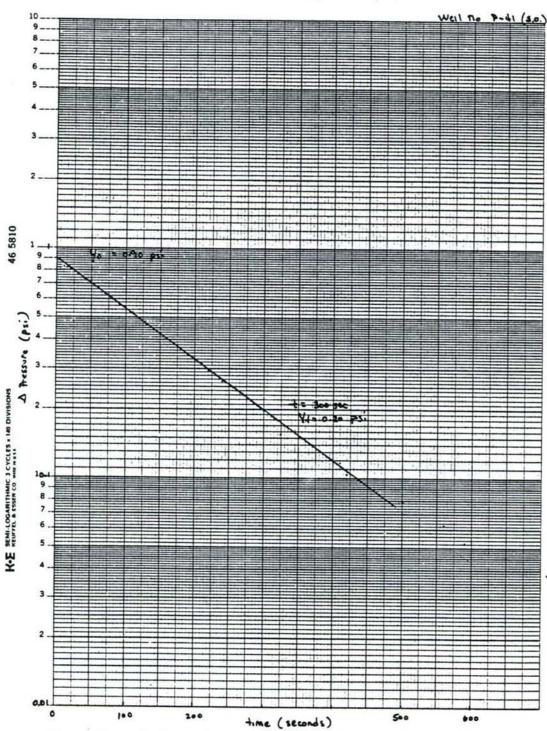
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	1/20	<b>- A</b>	- в			L	n Re/rw
	40.00	r de la generalisación de	1			****	
0.333	15.53	(0 + 1 )		1.5	·	2	2.01
	***************************************					were allowed to be	The second secon
· 40	\t	4+	14	In 40/4.	ŧ	K= 1/21	·×トッペン×イングナ
51 2.77'	. 100	0.81		.0123	•	3.9	9 x 10-3 cm / sec
50 2079	300	0.462		0050	X6		10-3 cm/sec
COMMENT		3.462	- 0.			1.6	The Confess
				E 9 0			· · ·
			4	any manana		O DOSEGNA NO. 140	
	8 8 8			g11 te			The the two transfers and the transfers



Data plot of elapsed time againse change in pressure for Well No. P-41 (SI phase)



Data plot of elapsed time againse change in pressure for Well No. P-41 (SO phase)

## ESE P. O. Box ESE GAINESVILLE, FLORIDA 32602 (904) 372-3318

CALCULATED BY DATE

SCALE	- 20
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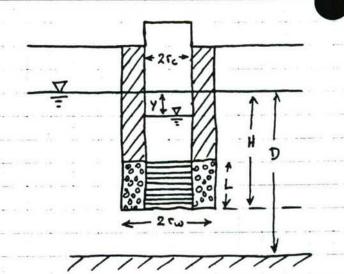
BOUWER & RICE (1976) METHOD

Well No P-44

Date 7-15-81

D+W-mp 22'2"

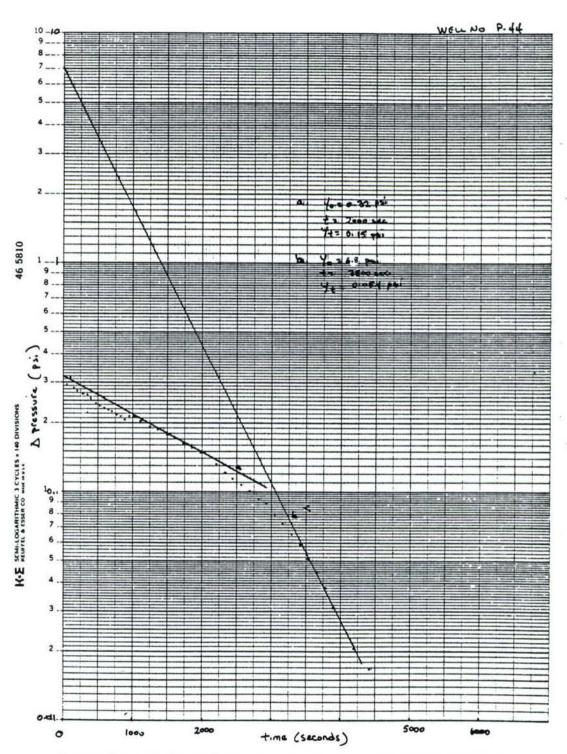
D+w-L5



Well A	edius		D	H	-1	-54-	(2/2L
casing	gravel pack				-	-	725
0.1667	6,333	27.83	27.83	27.83	: .	1.239	0.00103
- <b>(</b> )	1/50	A	8		2 10-2	L1	Re/rw
0.354	78.62			3	.s	3.1	372
. 40	.   +	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	TV	In 40/4	,	K = 50	X Logy X / Loy

7 18	· 40	sec .	- Y+	1/4 Ln 40/4+	K= 502 × Ln 30 × /2 Ln 1/2
a	0,739 ′	2000	0.346	0. 000 379	1.3 × 10-6 cm/sec
ъ	4.15,70'	3500	0,127	6.00138	1.5 ×10-4 cm/ Lec

Comments: Plot of time us AP shows two slopes. Early time data, up to 2000 sec, is calculated as an a (abone). Late time data is shown as b.



Data plot of elapsed time against change in pressure for Well No. P-44 (SI phase)

APPENDIX B
COMPUTER FILE LISTING

The data files listed below are in the UNIVAC 1108 at Aberdeen Proving Ground, Maryland.

<u>File</u>	Tier-2 Name	Date Entered
Chemical File, Phase II	ALSACGW81160	6/9/81
Groundwater Stabilization File, Phase II	ALSAGGS81154	6/3/81
Field Drilling File, Phase II	ALSAGFD81141	5/21/81
Map File, Phase I and Phase II	ALSAGMA81139	5/19/81

APPENDIX C
FIELD DRILLING FILE-PHASE I

J	1)	ALSAGF DROR FP-1	12920800219-1	FCLAC	16.5	00.00			- 3
J	5	AGF	2008022	LOLAC FOLAC	701	46000001		2YR4	
J		ALSAGE DESPER-1	180021	101	000	46 COLORUI		27846	9
_			12920R0021P-1	101	610	1000010001		2773	\$
_	5)		12920P0021P-1	FOL AC	0	DOLOR	10000	STRO	$\mathbf{x}$
J	(9.	ALSAGF	0021	FSIAC	•	2136801101	2000		
J	13	ALSAGF DPOREP-1	1272080021F-1	ESLAC		DAL THI		1010	
_	8	ALSAGFOROREP	1292080021F-1	ESLAC	0	ROBUSCS 01		2 2	2
J	6	ALSAGF DBOKFF-1	1292080021F-1	ESLAC	152		180	,	
_	10)	AL SAGF DEOREP-1	1252080021F-1	ESLAC	305	46HABL002	1001		
_	11)	ALSAGFOROREP-1	1292080021P-1	ESLAC	457	46HABL002	1181		
_	12)	ALSAGF DPORFP	1292080021P-1	ESLAC	610	46HABLO02	4BI		
<b>.</b>	13)	ALSAGFOROREP	1292080021F-1	ESLAC	762	46HABLO02	781		
٠.	14)	ALSAGF DPOREP-1		ESLAC	305	46MODIF 01		MOT	
٠.	15)	ALSAGF DEOREP-1		ESLAC	305	4 KMODIF01		CAL	
	16)	AL SAGF DBOREP	1292080021P-1	ESLAC	610	198MOD1F91		S	
		ALSAGF DEOREP	1292080021P-1	ESLAC	457	21		VET	
	18)	ALSAGE DROREP		ESLAC	457	305SCREN01			
	190	ALSAGF DBOREP-1		ESLAC	213	549SF1LT01			
	207	AL SAGF DRORE P-1		ESLAC		STKUP01	91CM		
٠.	213		1297780007P-10	ESNDA	0	30 COLOR01		SYRSE	æ
	. 22)	TEA.		ESWDA	152	46 COL OR 01		75YR700	-
•	23)			ESUDA	305	46COLOR01		10YR880	-
٠.	24)	200	97780007P-1	ESWDA	457	46COLORCI		10YR880	-
٠.	25)			ESUDA	610	46 COLORO1		75YR780	
	26)			ESADA	762	46COLOR01		75YR780	-
	200			ESUDA	914	46 COLOR01		75YR78	180
	200	ALSAGE DROKE P-10		ESWDA	0	30C0NSS01		E	
	201			ESNDA	152	46C0NSS01		VST	
	300			ESMDA	305	46C0NSS01		20	
	123	ALCACTORORED TO	1.480007P-1	ESMOA	457	46C0NSS01		ı	
	333	7		ESMUA	610	46C0NSS01		£	
	343	AL SAGEDHORED-10	01-4/00001/6	ESHUA	162	46C0NSS01		VST	
	35.)	SAGE DROPE P-1		ESMUA	616	46C0NSS01		20	
	36.)	ALSACEDROREP-10		ESHDA		101010016	914CM		
_	373		977800075-10	E SALDA		916800101			
-	38)		47780007P-10	4000	201	46HABLO32	SHE		
_	39)	ALSAGFDBCREP-10	778 JUN 77-10	T V C C C	657	ACHABLO02	1000		
-	40)			FSUDA	610	ACHARI ONS	1701		
-	41)		9778 30071-10	ESUDA	76.5	46HARLORS	2000		
-	42)	SAGF DRCP FP-1		ESVDA	014	A CHARLONS	2281		
_	43)		0	ESWDA	0	30MODIF 01		0	
_	44)	DRUPEF-1	12:77:0007F-10	ESWDA	315	464001F91		0	
<b>.</b> .	450		1247786007P-10	ESUDA	0	30M01SC01		DRY	
٠.	46)		0	ESUDA	152	4 CMOISCOI		VET	
٠.	6		0	ESWDA	305	46MOISCO1		VET	
	626	ALSAGE DRORFF-10	12977840070-10	ESMUA	45.7	4 KMOISCOI		DRY	
<b>.</b> .	6 6 6		-	ESWIDA	610	4 CMOISCPI		MOIST	
<b>.</b>	200		12277E20071-19	ETKDA	762	46M015C01		POIST	
٠,	210	ALSACF CHOPET-10	12977E3697F-12	ESWUA	610	4 F MOISCF1		WET	
٠.	521	ALSAGF DECHLP-10	12"771,96071-19 (	ESVEA	61.	305SCRENCI			
	200	ALSAGI DI PREFE-19	11.0777.00.711-10	F.C. U.A	i i	9145F1LT"1			
		AL SAGRETT STATES	1. 177	4					
				W		I KUP 1	11.5		

-	56)	ALSAGFOBORFP-1	77800	ESUDA	152		5	-
_	571	ALSAGFURUREP	12977800C7P-10	ESADA	305		5 5	
_	58)	ALSAGFOPOREP-1	77890	ESMUA	457		13	
_	59)	ALSAGFDROREP-1	1297780007P-10	ESWDA	610	10	נו	
_	(09)	AL SAGF DEOREP-10		ESWUA	762		H	+
_	61)	ALSAGE	1297780007P-19	-	614	46USCS 21	ט	
~	62)		12977800071-10	ESUDA	0	960LITHL01	RE	S
_	63)	ALSAGE	1287179363P-11	ESUDA	152	351 COLOR01	10	36
•	64)		1287179360F-11	ESVDA	152	0	S	0
-	62)	DROR	1287179360P-11	ш		DPTOTO	518CM	
_	(99	ALSAGFOBOREP-11	1287179360F-11	ш	0	1526ROUT01	100	
_	67)	ALSAGFDEOREP-11	1287179360P-11	ш	152	46HABLO02	198L	500 465
•	68)	ALSAGEDBOREP-11	1287179360P-11		152	351M01SC01		MOIST
	649	ALSAGE DROKEP-11	128/1/93608-11	ESUDA	*	RFUSLO	518CM	
•			11-10926111421	4000	0000	1323CRENUI		
	723	7 4	1287179360F-11	<b>J</b> L	613	0	MUCA	
	73)	ALSA	1287179360P-11	ESAD	0	518L1THL01	RE	\$10
	743	ALSA	1287179360P-11	ESWDA	0	518USCS 01	บ	
_	151	AL	1307679362P-12	ш	152	COLORD	2	77R68
-	76)	-	1307679362P-12	ESMOA	152		SC	_
-	(77		13076793629-12	<b>W</b> 1	305	4 FCONSSO	Σ.	
	78)	ALSAGFOROREP-1	1307679362P-12		457	610CONSS91	7 27.70	
	(6)	-	13076795628-12	ESEDA	c	0	108/08	
	81)	ALSAGFOROR FP-1	13076793620-12		0	2	R	ESID
_	82)	AL	1307679362P-12	ш	152	46HABLOO	1881	
~	83)	ALSAGFDBOREP-1	1307679362P-12	ESWDA	305	46HABLO02		
-	643	ALSA	13C7679362P-12	ESMD	457	6HABL00	12BL	
-	853	ALSAGF DBOREP-1	1307679362P-12	ESMDA	610	46HABLO02	9BL	
	861	ALSAGE DBOREP-1	07679362P-12	ESWDA	162	46HABLOUZ	1981	
•	100	ALSA	1-429261910	FAUDA	610	198MODIE01	1001	
. •	893	ALSAGFDBOREP-1	1307679362P-12	ESUDA	152	46M01SC0	0.0	DRY
~	606	ALSAGFOROREF-1	07679362P-12	ESWDA	305	762M01SC01	Ĭ	HOIST
•	(15	ALSAGF DPGREP-1	C7679362P-12	ESMDA			1067CM	
<b>-</b> .	921	A:	~	ESHUA	762	305SCREN91		
	931	ALSAGEDECKEF-12	16/95627-12	EVEDA FALSA	290	STRIPPOL	MJ 7U	
	(56	2 4	07679362F-12	ESUDA	0	0	1	1000
-	696	ALSAGF DEORFP-1	69279362P-13	ESWDA	152	655 COLORO	77	YR 78
_	116		13092743629-13	ESHUA		DPTOT	914CF	
-	626	COT.	13/1927 33621-13	ESMOA	0	3GROUT 0		77.00
-	166	124	13092733624-13	ESUDA	6	0	CZ.	ESID
	1001	۷ .	39279362P-13	ES.40 A	152	0	2561	
	1011	ALCACTORCECCO	13093791536713	4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	5 4 4	ACHABLO02	1281	
	1971	AL SAGFORDS FP-1	11277345P-13	4 1 1 5 L	616	2 C	188	
`~	104)	AL		ESADA	762	46HABLON2	1PL	
-	105)	ALSAGE	1260	ESUDA	457	46M0D1F01	ī	TO
•	106)	ALSAGFOROREP-13	3621-1	ESWUA	014	46.MODIF01	ž.	ROT
-	107)	AL.	1927 1936 E.F.	ESVEA	762	46MODIF 01	vo i	;
	Call Cont	ALSACEURORE P-13	120077051	E C C LA	100	TOUGH ON SO	2	7 7 7
		Att Chapte		4 1 1 1	44.7	CMOISC	-	
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113   ALSAGE DORREP-13   1309279352-13   SSUDA   SSU											
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ALAGE DIRREP-13 1109779567-13 ENUA ALAGE DIRREP-14 1122-4800095-14 ENUA 305 5762010R01 1143CH ALAGE DIRREP-14 1122-4800095-14 ENUA 305 762010R01 1143CH ALAGE DIRREP-14 1122-4800095-14 ENUA 305 7640481002 26H ALAGE DIRREP-14 1122-4800095-14 ENUA 305 764048100 200 144071001 305 805 800 1400 1400 1400 1400 1400 1400 1400	-	111		3	3092793626	m	ESUDA	762	46M01SC01		
ALSAFER PORTER=13   1302773567-13 ESUAD   55 5795 FELTO     ALSAFER PORTER=14   1302773567-13 ESUAD   55 795 FELTO     ALSAFER PORTER=14   1302773670-13 ESUAD   55 795 FELTO     ALSAFER PORTER=14   13027773670-13 ESUAD   55 795 FELTO     ALSAFER PORTER=15   1307773559-15 ESUAD   57 795 FELTO     ALSAFER PORTER=15   1307773559-15 ES	٠.	1123		3	309279362	2	ESADA	1000		914CM	
ALSAGE   DRORE   1   1   1   1   1   1   1   1   1		113	7	. 3	3092793621	-13	ESUDA	610			
ALSAGE BORREP-14   132248 BOODSP-14   ENDA   0 9140SCS   0 1		111		0.	3092193621	-13	ESUDA	335	579SFILT01		
		115		0.	3092793621	-12	ESUDA	•		92CF	
ALSAGEBOREP-14   12224800039-14   5304   152   762000001   174307   17430	- ~	117)	3	0.4	1224800046	21.0	E SWID	2 0			כר
		110)	9.7	. 4	2224800035	41-0	FAUDA	305	7625010801		EVDED
ALSAGEBOREP-14   1322480003P-14   ESUDA   1057 76[11.0]   1143CH     ALSAGEBOREP-14   1322480003P-14   ESUDA   1057 76[11.0]     ALSAGEBOREP-14   1322480003P-14   ESUDA   1057 76[11.0]     ALSAGEBOREP-14   1322480003P-14   ESUDA   1057 76[11.0]     ALSAGEBOREP-14   1322480003P-14   ESUDA   1057 46HABLOOZ   26RL     ALSAGEBOREP-14   1322480003P-14   ESUDA   1057 46HABLOOZ   1057     ALSAGEBOREP-14   1322480003P-14   ESUDA   1057 1057   1057     ALSAGEBOREP-15   13377979359P-15   ESUDA   1057   1057   1057     ALSAGEBOREP-15   13377	-	119)	1	,	3224800031	-14	FOUND	152	46.CONSON		0041
ALSAGEDOREP-14 1322460037P-14 ESUDA 1067 76FILL 01 ALSAGEDOREP-14 1322460037P-14 ESUDA 173LITHU01 ALSAGEDOREP-14 1322460037P-14 ESUDA 155 46HABLOO2 26BL ALSAGEDOREP-14 1322460037P-14 ESUDA 155 46HABLOO2 18BL ALSAGEDOREP-14 1322460037P-14 ESUDA 155 46HABLOO2 18BL ALSAGEDOREP-14 1322460037P-14 ESUDA 155 46HABLOO2 18BL ALSAGEDOREP-14 1322460037P-14 ESUDA 155 19HABLOO2 18BL ALSAGEDOREP-14 1322460037P-14 ESUDA 156 19HABLOO2 18BL ALSAGEDOREP-15 13473773337P-15 ESUDA 0 9140F1010 19CR ALSAGEDOREP-15 1347377333P-15 ESUDA 0 9140F1010 19CR ALSAGEDOREP-15 1347773337P-15 ESUDA 0 9140F1010 19CR ALSAGEDOREP-15 1347773337P-15 ESUDA 0 9140F1010 19CR ALSAGEDOREP-15 1347777333P-15 ESUDA 0 9140F1010 1	-	120)	AL	4	3224800031	-14	ESVDA	-	)	1143CH	
ALSAGENGREP-14 1322480003P-14 ESUDA 0 1143LITHU01	~	121)	AL	4	3224800035	-14	ESUDA	1067	76FILL 01		
ALSAGEDROREP-14 1322480003P-14 ESUDA 155 46H8L002 26RL ALSAGEDROREP-14 1322480003P-14 ESUDA 305 46H8L002 26RL ALSAGEDROREP-14 1322480003P-14 ESUDA 45FHRL002 26RL ALSAGEDROREP-14 1322480003P-14 ESUDA 46HRL002 26RL ALSAGEDROREP-14 1322480003P-14 ESUDA 162 46HRL002 36RL ALSAGEDROREP-14 1322480003P-14 ESUDA 162 46HRL002 18RL ALSAGEDROREP-14 1322480003P-14 ESUDA 105 46HRL002 18RL ALSAGEDROREP-14 1322480003P-14 ESUDA 105 46HRL002 18RL ALSAGEDROREP-14 1322480003P-14 ESUDA 105 46HRODEO 18RL ALSAGEDROREP-14 1322480003P-14 ESUDA 105 19HRODEO 18RL ALSAGEDROREP-14 1322480003P-14 ESUDA 11402CS 01 1574RP ALSAGEDROREP-14 1322480003P-14 ESUDA 11402CS 01 1574RP ALSAGEDROREP-15 1347797353P-15 ESUDA 0140PL0101 91CR ALSAGEDROREP-15 1347797353P-15 ESUDA 0140PL0102 14RL ALSAGEDROREP-15 1347797353P-15 ESUDA 0140PL0102 14RL ALSAGEDROREP-15 1347797353P-15 ESUDA 0140PL0102 14RL ALSAGEDROREP-15 1347797353P-15 ESUDA 0505CREDO 18RL ALSAGEDROREP-15 134779	_	122)		4	3224800035	-14	ESUDA	0	91GROUT01		
ALSAGE BORGE F-14  1322480003P-14 ESUDA 305 464480002 268L  ALSAGE BORGE F-14  1322480003P-14 ESUDA 455 464480002 268L  ALSAGE BORGE F-14  1322480003P-14 ESUDA 455 464480002 268L  ALSAGE BORGE F-14  1322480003P-14 ESUDA 762 464480002 18L  ALSAGE BORGE F-14  1322480003P-14 ESUDA 762 764480002 18L  ALSAGE BORGE F-14  1322480003P-14 ESUDA 762 764001F01 0RY  ALSAGE BORGE F-14  1322480003P-14 ESUDA 762 3034015C01 0RY  ALSAGE BORGE F-15  1324797353P-15 ESUDA 914C0NSO 196CH  ALSAGE BORGE F-15  1347797353P-15 ESUDA 014C0NSO 196CH  ALSAGE BORGE F-15  1347797353P-15 ESU	_	123)	-	4	3224800035	4	ESUDA	0			RESID
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ALSAGE DRORE P-14 1322480003P-14 E SUDA 457 464480002 278L  ALSAGE DRORE P-14 1322480003P-14 E SUDA 762 464480002 18L  ALSAGE DRORE P-14 1322480003P-14 E SUDA 762 464480002 18L  ALSAGE DRORE P-14 1322480003P-14 E SUDA 762 904001F01 07 07 07 07 07 07 07 07 07 07 07 07 07	~	125)		4	3224800035	-14	ESUDA	305	46HABL002	2681	
ALSAFDROREP-14 1322480003P-14 ESWDA 611 46448L002 98L  ALSAFDROREP-14 1322480003P-14 ESWDA 156 4648L002 18L  ALSAFDROREP-14 1322480003P-14 ESWDA 156 464001F01 07L  ALSAFDROREP-14 1322480003P-14 ESWDA 159 908001F01 07L  ALSAFDROREP-14 1322480003P-14 ESWDA 159 908001F01 07L  ALSAFDROREP-14 1322480003P-14 ESWDA 150 908001SC01 07L  ALSAFDROREP-14 1322480003P-14 ESWDA 162 908001SC01 07L  ALSAFDROREP-15 1322480003P-14 ESWDA 17535F1LT01 91CH  ALSAFDROREP-15 1327979353P-15 ESWDA 0740P107001 96.0CH  ALSAFDROREP-15 1347979353P-15 ESWDA 0740P10701 91.0CH  ALSAFDROREP-15 1347979353P-15 ESWDA 0740P107001 91.0CH  ALSAFDROREP-16 1347979353P-15 ESWDA 0740P107001 91.0CH  ALSAFDROREP-16 134799353P-15 ESWDA 0740P107001 91.0CH  ALSAFDROREP-16 134799353P-15 ESWDA 0740P		126)	_	4	3224800035	-14	ESNDA	457	46HABL002	27BL	
ALSAGE DROREP-14 1322480003P-14 ESUDA 762 4648BL002 581  ALSAGE DROREP-14 1322480003P-14 ESUDA 152 464001F01 0 CAL  ALSAGE DROREP-14 1322480003P-14 ESUDA 152 464001F01 0 CAL  ALSAGE DROREP-14 1322480003P-14 ESUDA 152 503401SC01  ALSAGE DROREP-14 1322480003P-14 ESUDA 152 503401SC01  ALSAGE DROREP-14 1322480003P-14 ESUDA 152 503401SC01  ALSAGE DROREP-14 1322480003P-14 ESUDA 762 5058REN01  ALSAGE DROREP-15 1322480003P-14 ESUDA 01434CS 01  ALSAGE DROREP-15 1322480003P-14 ESUDA 01434CS 01  ALSAGE DROREP-15 1322480003P-14 ESUDA 01434CS 01  ALSAGE DROREP-15 1337979353P-15 ESUDA 01448L002 198L  ALSAGE DROREP-15 1337979353P-15 ESUDA 019401001  ALSAGE DROREP-15 1337979353P-15 ESUDA 019401002 198L  ALSAGE DROREP-15 1337979353P-15 ESUDA 019401002 198L  ALSAGE DROREP-15 133797935P-15 ESUDA 019401000 191CM  ALSAGE DROREP-15 133797935P-15 ESUDA 01940100 191CM  ALSAGE DROREP-15 194010000000000000000000000000000000000	-	127)		4	3224800035	-14	ESUDA	610	46HABL002	186	
ALSAGFORGREP-14 1322480003P-14 ESWDA 514 464M01F01 104 ALSAGFORGREP-14 1322480003P-14 ESWDA 515 46M001F01 CALALSAGFORGREP-14 1322480003P-14 ESWDA 515 503M01SC01 OP ALSAGFORGREP-14 1322480003P-14 ESWDA 515 503M01SC01 OP ALSAGFORGREP-14 1322480003P-14 ESWDA 515 503M01SC01 OP ALSAGFORGREP-14 1322480003P-14 ESWDA 762 305KRED101 OP ALSAGFORGREP-14 1322480003P-14 ESWDA 014COLOR01 OP ALSAGFORGREP-15 134797953P-15 ESWDA 0914COLOR01 OP ALSAGFORGREP-15 134797953P-15 ESWDA 0914COLOR01 OP OP ALSAGFORGREP-15 134797953P-15 ESWDA 0914COLOR01 OP	• .	128)		4	3224800035	-14	ESUDA	762		581	
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ALSAGF DBOREP-15  1347979553P-15 ESWDA 0 914COLOR01  ALSAGF DBOREP-15  1347979553P-15 ESWDA 0 914DT0101  ALSAGF DBOREP-15  1347979553P-15 ESWDA 0 914DT0101  ALSAGF DBOREP-15  1347979553P-15 ESWDA 0 906LITHL01  ALSAGF DBOREP-15  1347979553P-15 ESWDA 152 46HABL002  ALSAGF DBOREP-15  1347979553P-15 ESWDA 457 46HABL002  1347979553P-15 ESWDA 457 46HABL002  ALSAGF DBOREP-15  1347979553P-15 ESWDA 457 46HABL002  1347979553P-15 ESWDA 467 46HABL002  198L  ALSAGF DBOREP-15  1347979553P-15 ESWDA 40 46HABL002  198L  ALSAGF DBOREP-15  1347979553P-15 ESWDA 610 46HABL002  198L  ALSAGF DBOREP-15  1347979553P-15 ESWDA 610 46HABL002  148L  ALSAGF DBOREP-15  1347979553P-15 ESWDA 610 46HABL002  148L  ALSAGF DBOREP-15  1347979553P-15 ESWDA 610 96DSCREN01  ALSAGF DBOREP-15  1347979553P-15 ESWDA 610 96DSCREN01  ALSAGF DBOREP-15  1347979553P-15 ESWDA 610 96DSCREN01  ALSAGF DBOREP-15  1347979553P-15 ESWDA 610 305SCREN01  ALSAGF DBOREP-15  1347979553P-15 ESWDA 610 96DSCS 01  ALSAGF DBOREP-15  1347979553P-15 ESWDA 610 96DSCS 01  ALSAGF DBOREP-15  1347979553P-15 ESWDA 610 96DSCS 01  ALSAGF DBOREP-16  134797979553P-15 ESWDA 610 96DSCS 01  ALSAGF DBOREP-16  1347979553P-16  1347979553P-15  ALSAGF DBOREP-16  1347979553P-15  ALSAGF DBOREP-16  1347979	٠,	139)		•	3224800035	-14	ESMDA	0	1143USCS 01		บ
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ALSAGF DEOREP-15	~	146)	ALSAGF DBOREP-1	5	3479793536	-15	ESUDA	305	46HABLO02	1481	
ALSAGFORGREP-15 1347977353F-15 ESWDA 610 46HABLOD2 19BL ALSAGFORGREP-15 1347979353F-15 ESWDA 762 46HABLOD2 12BL ALSAGFORGREP-15 1347979353F-15 ESWDA 914 46HABLOD2 14BL ALSAGFORGREP-15 1347979353F-15 ESWDA 915 19BMOISCO1 14BL ALSAGFORGREP-15 1347979353F-15 ESWDA 305 6095F1LT01 ALSAGFORGREP-15 1347979353F-15 ESWDA 305 6095F1LT01 91CM ALSAGFORGREP-15 1347979353F-15 ESWDA 305 6095F1LT01 ALSAGFORGREP-15 1347979353F-15 ESWDA 305 6095F1LT01 ALSAGFORGREP-16 1347979353F-15 ESWDA 305 6095F1LT01 ALSAGFORGREP-16 1347979353F-16 ESWDA 305 4570LOR01 ALSAGFORGREP-16 13428779353F-16 ESWDA 305 4570LT01 ALSAGFORGREP-16 13428779353F-16 ESWDA 305 4570LT01 ALSAGFORGREP-16 1342877353F-16 ESWDA 305 4570LT01 ALSAGFORGREP-16 1342877353F-16 ESWDA 155 4570LT01 ALSAGFORGREP-16 13442877353F-16 ESWDA 155 4570LT01 ALSAGFORGREP-16 1542877353F-16 ESWDA 155 4570LT01 ALSAGFORGREP-16 1542877353F-16 ESWDA 155 457	-	147)	ALSAGF DROPEP-1	5	347979353F	-15	ESUDA	457	46HABL002	2981	
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ALSAGFDROREP-15 1347979353P-15 ESWDA 305 610M0ISC01 ALSAGFDROREP-15 1347979353P-15 ESWDA 305 610M0ISC01 ALSAGFDROREP-15 1347979353P-15 ESWDA 610 305SCREN01 ALSAGFDROREP-15 1347979353P-15 ESWDA 305 6995F1LT01 ALSAGFDROREP-15 1347979353P-15 ESWDA 0 960USCS 01 ALSAGFDROREP-16 1342879353P-16 ESWDA 152 46COLOR01 ALSAGFDROREP-16 1342879353P-16 ESWDA 3CS 457COLOR01 ALSAGFDROREP-16 1342879353P-16 ESWDA 3CS 457COLOR01 ALSAGFDROREP-16 1342879353P-16 ESWDA CONSS01 ALSAGFDROREP-16 1342879353P-16 ESWDA 15: 46HARLORD SOPL	-	1501		5 1	3479793530		ESUDA	914	46HABLO02	1481	
ALSAGFDROREP-15 1347977353P-15 ESNDA 305 610MOISCO1 ALSAGFDROREP-15 1347977353P-15 ESNDA 610 305SCREN01 ALSAGFDROREP-15 1247977953P-15 ESNDA 305 6995FLT01 ALSAGFDROREP-15 1347979353P-15 ESNDA 0 960USCS 01 ALSAGFDROREP-16 1342879353P-16 ESNDA 152 46COLOR01 ALSAGFDROREP-16 1342879353P-16 ESNDA 3CS 457COLOR01 ALSAGFDROREP-16 1342879353P-16 ESNDA 0 960USCS 01 ALSAGFDROREP-16 1342879353P-16 ESNDA 0 2446R0UT01 ALSAGFDROREP-16 1342879353P-16 ESNDA 0 2446R0UT01 ALSAGFDROREP-16 1342879353P-16 ESNDA 0 3CP 46HARLOR0 3CP 46HARLORD 3CP 46HAR	-	151)		5 1	347979353F		ESUDA	٥	198M0ISC01		DRY
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219) ALSAGF CPUREF-18	1	365793540-18	ESMUA	152	46HAELOU2	1001	

	221)	ALSAGF DROREP-1	36579354P-18 F	ACUA	45.7			
	222)	ALSAGF DBOREF-1	1336579354F-18 E	SEDA	610	46HABLOUZ	2201	
	223)	ALSAGF DBOREP-1	36579355P-18 E	SUDA	152	46MODIF 01	1022	c
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	2271	ALSAGE DEUKLF-18	54P-18	ESWDA	305	05SCRENO		
	228)	SAGE DRORED-1	36577354P-18	ESMDA	558	0		
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	230)	SAGFORORFP-1	۱ د	V O N	0			CL
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	232)		- L	AUNG	305	198COLOR01		7YR68
	2333	SAGF DROR EP-1		AUN'S	019	320C0L0R01		2YR5
	234)	SAGF DBOR EP-1	9780016P-19 F	NO NO	152	351C0NSS01		ST
	235)	SAGF	29780016P-19 F	FAUDA	019	SZUCONSSOI		VST
	236)	ALSAGF DBOREP-19	29780016P-19	FOUND	410	185711 01	930CM	
	237)	SAGF DBOREP-1	29780016P-19	ESUDA		1226BOUT 01		
	238)	SAGF DHOREP-1	9780016P-19	ESUDA		9301 1THI 01		
	239)	SAGF DBOREP-1	9780016P-19	ESUDA		, 4	1011	KES 10
	240)	ALSAGF DBOR EP-19	297R0016P-19	SUDA	305	46HABI 002	1081	
	241)		3 6	ESWDA	5	46HABL002	100	
	1747	SAGF DBOR EP-1	1329780016P-19 ES	SUDA	610	46HABLO02	781	
	2400	SAGFOBOREP-1	9 E	SUDA	762	46HABL002	981	
	2451	ALSAGE UBOREP-19	3 E	SUDA	152	46MODIF 01		0
	246)	SAGE	9 E	SUDA	152			VET
	2473	SAGF DROREP-1	13297800167=19 ES	SWDA	305	196MODIF01		0
	248)		9 6	AUNA	610	195MOISCOI		VET
	2493	SAGF DBOR EP-1	9780016P-19	ESUDA	610	SOSMOTSCOL		
	250)	SAGF DBOREP-1	29780016P-19	ESUDA	610	05SCRFN		
4.5	(162	SAGF DBOREP-1	9780016P-19	ESWDA	457	57		
	253	ALSAGE DBOKEP-19	29780016P-19	ESVDA		STKUP01	91CM	
	2543		19 E	ESUDA	0	930USCS 01		כר
	2553	AL SAGE DROPE PLA	w 1	SLAC	152	46COLOR01		5YR5
	256)	ALSAGE DRORED - 2	2	ESLAC	305			5YR22
	257)	ALSAGF DRORFP-2	2 0	SLAC	610	46COLORU1		10YR68
	258)	ALSAGFOROREP-2	7-10	LSLAC		DPTOT	655CM	
-30	2591	ALSAGF DROREP-2			6/6	122CBOUT01		
17E)	569)	ALSAGF DROREP-2	P-2 E		o c	O I I I I I		-
	261)	SAGF DROREP-	5780017P-2 E		152	46HABL002	1281	T SID
	7077	SAGE DEOREP-	05780017P-2 E		305	6 HABLOO	3981	
roinile	2641	ALSAGE DEOREFIE	5780017P-2 E		457		17RL	
5/35	2661	CAST DECKEP	05780017r-2 E		610	46HABL002	10PL	
	(99)	SACTUROR P.	2		152			JET.
	2671	ALCADE DE DE CELE	05780517P-2 E		152	A6MODIF01		(2)
11/2/2		١.	·		152	46MODIF91	_	2
(0.00		ALSAGERPONED T	15057890178-2 ESI		335	46MODIF91		
		ALSAGFUNDERP .:	ه له		365	46.M01.SC91	_	VET
	_	SAGFOPOPEP	0.000111111111111111111111111111111111	25.60		46 MODIF 01	_	HOT
		ALSAGE DROREP-5	,,			AFMODIF 01		CAL
••		ALSAGF DRORP F-	157800171-3		100	4 FMODIFOI	_	
	_	ALSAGFUPURLE -:	57F0017F-2			1005 COM 34	•	17
	753	ALCAST DRUBEP-	C-1110-111-2			10.1100111		-
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2YR46 0

275) ALSAFERDREE—2 1307580177-2 ESLAC 774 30556RFR101 POT 779 1815AFR1101 POT 779 1815
ALGAGEDORREP—2 1305780017P—2 ESLAC 274 3655CREND ALGAGEDORREP—2 1305780017P—2 ESLAC 122 4575E1170 122CM ALGAGEDORREP—2 1305780017P—2 ESLAC 122 4575E1170 122CM ALGAGEDORREP—2 1305780017P—2 ESLAC 122 4575E1170 122CM ALGAGEDORREP—2 1305780017P—2 ESLAC 0 650SCS 01 37740017P—2 ESLAC 0 650SCS 01 37740017P—1 ESCAC 0 650SCS 01 37740017P—1 ESC
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275) 2771 2771 2771 2771 2771 2771 2771 277

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J	331)	AL	1448479339P-21	w	610	46HABL002	3281	
_	332)		1498479339F-21	ш	762	46HABLOD2	230L	
	333)		1498479335F-21	ESMOA	914	46HABLO02	26BL	
٠.	334)		1498479339F-21	ESUDA	305			MOT
	4460	ALSACTURORI PEZI	14984/9339F-21	LSWDA	152	SUSMOISCOI		DRY
	337)	A	- d628	FSUDA	195	REUSEUL	1 DE 3CM	DRY.
_	338)	100	1498479339P-21	ESWDA	9	296SCREN91	-	
-	339)	0.00	14984793399-21	ESUDA	305	56SFILT		
_	340)		1498479339P-21	w		STKUP01	95CM	
-	341)		1498479339P-21	w	0	1063USCS 01		נו
_	345)		1453980023P-22	w	152	198COLOR 01		2YR36
٠.	343)	ALSAGF DRORE P-22	1453980023F-22	w	457	46C0L0R01		2YR46 0
	2000		1453980023F-22	w	610	46C0L0R01		~
	245	ALSAGE DEOREDES	14559800238-22	<b>.</b> .	162	4600000		77R78 0
	347)	ALSAGEDROREP-2	14537800237-22	FSIAC	201	DETOTOL	M C 0 0 0	121
_	348)	ALSAGFDBOREP-22	1453980023P-22		762	46FILL 01		
_	349)	ALSAGFOBOREP-2	14539800237-22	. w	0	3 GROUT		
-	350)	ALSAGF DBOREP-2	1453980023P-22	ESLAC	0	808LITHL91		RE\$10
-	351)	ALSAGF DBOREP-2	1453980023F-22	ш	152	46HABLO02	25BL	
	352)	ALSAGF DBOREP-22	14539R0023F-22	w	305	6HABL00	18BL	
٠.	353)	AL SACF DROREP - 22	14539800238-22	w 1	457	46HABLOD2	RBL	
	355	ALSAGEDRORED-S	14539800238-22	FOLAC	019	46HABLOUZ	196	
	356)	ALSAGFORORFP-2	14539800237-22		305	A C MODIE 01	7000	TPC
-	357)	ALSAGFOBOREP-2	1453986023P-22		305	46M0D1F01		TRCL
~	358)	ALSAGF DBOREP-22	14539800238-22	ш	610	46MODIF01		HOT
	359)	ALSAGF DBOR EP-22	1453980023P-22	w	305	351M01SC01		VET
	360)	DBOREP-2	1453980023P-22	W 1	762	46M01SC01		DRY
	1621	ALSAGE DEOREP = 22	14559800238-22	ESLAC	166	SUSSCRENOI		
	363)	ALSAGEDEOREP-22	14539800230-22		613	STKIIPUI	MULTO	
_	364)		53980023P-2		0	80805CS 01		73
_	365)	ALSAGF DBOREP-23	14246793399-23		152	~		10YR88
-	366)	11.00	1424679339P-23	ESWDA	762	198COLOR01		2YR48
~	367)		14246793391-23	ESVDA	1067	503C0L0R01		SYRGA
٠.	368)	ALSAGF DROREP-23	14246793399-23	ESMUA	305	55CONSS		_;
	3703		14246 / 93397 = 23	ESUDA	1001	SUSCONSSOI	16705	
	3711	ALSAGE DECREP-23	14246791311	٠,	1524	ACETI 01	10101	
	372)		14246793391-23		0	2056ROUT01		
-	373)	ALSACFDROREP-2	14246793399-23	<b>"</b>	0	1570LITHL01		RESTO
-	374)	ALSACFDBOREP-2	14246793391-23	ESUDA	152	46HABL002	29BL	
_	375)	ALSAGF DROPFP-2	14246793395-23	ESMDA	202	46HABL002	39BL	
	376)	ALSAGE DEOPEP-2	14244 793391-23	w	457	46HABLO02	SORL	
	377)	ALSAGE	246743391	ESMOA	613	46HABLO02	2581	
	1270	A .	14.746 / 75591 - 25	L: UIA	166	46HABL002	15HL	
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	37.13		14-46743501-23	E CUDA	1214	0	ISBI	
_	382)	ALSAGFDROREP-23	14246793391-23	FSULIA	1372	00	23PL	
-	31.53	ALSAGE DEOPT P-23	1333.	ESMEA	1524	46. HABLORZ	23BL	
-	384)	ALSAGFOFCHIF-, 3	14.46.7.33.01 -23	Willian 9	. 11.	TOURCESTON		٥
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436	ALSAGE DE	REP-7	2.89800141-2	FSWL	914	51 COL	
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RESID

1311CM

LM MOIST

91CM

O	ALSAG	ALSAGFDBOREP-1	P-1	1292080021P-1	1 ESLAC	152	46COLOR01	OROI	2YR46	0 9		
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		441)		P-26	1428980014P-2	P-26	ESWDA		0010101	1570CM		-
(	٠.	445)		956	N	92-0	ESUDA	1524	46FILL 01			0
		443		2-26	Cu I	92-	ESWDA	0	05GR0U1			0
		4 4 4		92-50	2898001	-26	ESMDA	0			RES 1D	0
C		400	ALSAGE DROBED - S	97-0	N		ESUDA	152	46HABLO02	23BL		0
,		4473		9-26	14289860147-26		ESUDA	305	46HABL002	1493		0
	_	448)		90-0	vo		LONDA	156	46HABL002	1PBL		0
ر	J	449)		92-0	1428980014P-26		FOUDA	019	46HARLOUZ	26BL		0
	J	450)		. 92-0	10		FOUND	201	46HABLOUZ	3581		0
	_	451)	AL	-26	14289800146		E CUDA	1067	4 CHABLOUS	7362		0
C	_	455)	AL	-26	1428980014F-26		ESUDA	1219	46HARIOD2	2781		0 0
	_	453)	AL	-26	1428980014P-2		ESWDA	1372	46HARL092	2641		٠.
(		454)	AL	26	1428980014P-26		ESUDA	1524	46HABL002	728I		0 0
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1	٠,	456)	AL	-26	1428980014P-26		ESWDA	457	457M0D1F01			
c		000		-26	428980014P-26		ESUDA	914	351M0DIF01		0	0
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C		4611	7	97-	428980014P-26		ESUDA	1219	05SCREN			0
)		4623	AL SAGE DRORED - 26	100	200		ESWDA	305	1219SFILT01			0
		4633	4	90-1	426980014F-26		ESUDA		STKUP	76CM		0
0	_	464)	A	101	4977000146-25		ESWUA		OUSCS		บ	0
	_	465)	ALSAGFOROREP-2	-27	3877800160-27		FOUND	701	46C0L0R01		2YR 58	0
	J	466)	ALSAGFDBOREP-27	-27	3877800169		SUDA	200	46C0L0R01		7 X 7 Z Z	0 0
0	_	467)	ALSAGF DBOREP-27	-27	8001		ESUDA	610	46COLORO1		74070	٥ د
	_	468)	ALSAGFOROREP-27	-27	387780016P		SUDA	457	4 CONSENT		VCT 10	
(		4691	ALSAGFDBOREP-2	-27	387780016P-2	-27	SUDA	610	46C0NSS01		L S	
)		470	ALSAGF DROREP-27	-27	387780016P-27	-27	SUDA		<b>DPT0101</b>	671CM		0
		4727	ALSAGE DROKEP-27	-27	387780016P-2	-27	SWDA	655	-			0
C		4733	ALSAGE DEOREP-27	-27	387780016F-2	- 1	SUDA	0	183GROUT01			0
)		474)	ALSAGEDROREP-2	127	387786016P-2		ESVDA	0 .	671LITHL01		RES 10	0
	_	4751	SAGFORORFP	-27	3877800165-2	127	SUDA	152	46HABL002	1081		0
3	_	476)	ALSAGF DROREP-2	-27	387780016P-2	272	4000	000	46HABLOUZ	1881		0
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48) ALSAGFDFOREP-3 1299279349F-3 ESWDA 457 46USCS 01 49) ALSAGFDFOREF-30 13742R0005F-30 ESVBA 0 30COLOR01	547			12902793405-3	ESWUA	0	57USCS		ರ
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	( 551)	ALSAGFDROKEP-3	1374	280005P-30	-	305	46.001.0801		SEVDA	5
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	( 224)	ALSAGFOROREP-3		2800059-30				655CM	2	0
	( 222)	ALSAGFDEOREP-3	0 1374	2P 00 05P-30		625	30FILL 01			0
٥	1929	ALSAGFOROPEP-3		1374280C05P-30	w	O	3GROUT			0
	557)	ALSAGF DRONEP-3		2FC005P-30		152	46HABL002	74BL		0
(	558)	ALSAGF DBOREP - 3		280005P-30	ч	305	46HABL002	24PL		0
c	5591	ALSAGFDBOREP-3	-	374280005P-30	ш	457	46HABLO02	2881		0
	260)	ALSAGF DROREP - 3	1374	74280005P-30		619	46HABLO02	SORL		0
(	561)	ALSAGF DBOREP-3	1374	280005P-30		457	152MODIF01		0	0
5	562)	ALSAGF DEOREP-3	1374	280005P-30		c	30M01SC01		DRY	0
	563)	ALSAGFOROREP-3	1374	280005P-30	ш	152	46M01SC01		DRY	0
	564)		1374	2800058-30		305	46MOISC01		DRY	0
	(696		-	374280005P-30		457	152M0ISC01		DRY	0
9	266)		13	74283005P-30	ESUDA	0	640RFUSL01	€55CM		0
(	267)		1	374280005P-30		320	305SCREN01			0
2	1896			374280005P-30		213	411SF1LT01			0
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	572)	ALSAGFDBOREP-3		374280005P-30		305	152USCS 01		E E	0
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C	9	608)	ALSAGFDROREP-5	1296679351P-5	ESMDA	.716	46C0L0R01		27858	0
	9	6023	ALSAGFUROREP-5	1296679351P-5	ESUDA	162	1520010801		24868	0 0
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C		6141	ALSAGF DEOREP - 5	1296679351P-5	ESWDA	259	46HABLO02	27BL		0
,	.9	615)	ALSAGF DBOREP-5	1296679351P-5	ESWDA	411	46HABL002	14BL		0
	9	616)	AL SAGF DROREP-5	1296679351P-5	ESNDA	564	46HABL002	11RL		0
C	9	617)	ALSAGF DROREP-5	1296679351P-5	ESUDA	716	46HABL002	13BL		0
	9	618)	ALSAGFOROPEP-5	1296679351P-5	ESWDA	762	46HABL002	1281		0 0
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د		6243	ALSAGE DECREE	1296679351P-5	ESUDA	305	610SF1LT01			0
		625)	AL SAGF DROREP - 5	1296679351P-5	ESWDA		STKUP01	81CM		0
C		626)	ALSAGFDBOREP-5	1296679351P-5	ESUDA	0	914USCS 01		r C	0
)	9	627)	ALSAGF DBOREP-6	1261279352P-6	ESWDA	152	351COLOR01		7YR68	0
	9	628)	ALSAGFDROREP-6	1261279352P-6	ESUDA	610	46COLOR01		2YR46	0
0	9	629)	ALSAGFDBOREP-6	1261279352P-6	ESNDA	762	46COLOR01		7YR 78	0
)	9	630)	ALSAGF DBOREP-6	1261279352P-6	ESHDA	152	46C0NSS01		20	0
	9	631)	ALSAGFDBOREP-6	1261279352P-6	ESWDA	302	46C0NSS01		<b>X</b>	0
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)		636)	ALSAGFDROREP-6	1261279352P-6	ESWDA	152	46HABLO02	28BL		0
	9	637)	AL	1261279352P-6	ESADA	305	46HABL002	27BL		0
0	9	638)	AL	1261279352F-6	ESMDA	457	46HABLO02	19BL		0
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	152	152	152	152	152	305	365	365	305	305	305	457	457	457	457	457	454	610	610	019	610	610	610	762	762	762	762	762	762	914	914	414	916	914	914	1067	1067	1067	1067	1067	1067	1219	1219	1210	121	121	161
	ESWDA	FONDA	FOLDA	ESKDA	ESPDA	ESKDA	ESUDA	ESWDA	ESLDA	ESMUA	ESUDA	ESMDA	ESUDA	ESUDA	ESUDA	ESWDA	ESUDA	LSMDA	FOUNDA	FOURT	FSUDA	ESWDA	ESWDA	ESNDA	ESUDA	ESWDA	FSUDA	ESUDA	ESVDA	ESMDA	ESKDA	ESHUA	FSUDA	ESUDA	ESWDA	ESWDA	ESUDA	ESHUA	FSUDA	ESLIA	ESWLA	ESWUA	ESEDA	EST DA	ESEDA	A STATE	4
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000	LSAGFDBOREC	ALSAGEDBORECTSA	SAGFORCREC	LSA	LSAGFDBOREC	_	LSAGFUBOREC	SACFDBOR	ALSAGF DRUREC-3A	ALSAGF DBOREC-3A	AGFDBOREC	SAGFDBOREC	SAGFOROREC	ALSAGE DEOREC - 3A	AGFOROREC	ALSAGF DBOREC-3A	ALSAGF DBORE C-SA	nu	ALSAGEDBORECTA	ALSAGEDRORECTA	AGFDHOREC	4	ALSAGF DB OR EC-3A	ALSAGFDBOREC-3A	ALSAGF DBOREC-3A	ALSAGEDBOREC-3A	AGFOROREC	ALSAGFDBOREC-3A	AGFUROREC	SAGFUBOREC	ALSAGFOBOREC-3A	ALSAGE DEUKEC - SA	ALSAGEDRORECTSA	SAGFOROREC	SAGFOROREC	AGFDBOREC	ALSAGE UBUREC - SA	ALSAGEDHORECTSA	LSAGFDFORFC	LSAGFDBUPFC	ALSAGF DHOFEC-3A	_	LSAGFUPPPEC	LSAGFDFOREC	LSAGFDROREC	ALCACTOROPECTA	SAU DOUR LL
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280)	ALSAGFUNDREC	32481015C-3A E	SWDA	13/2	43L11HL01		KESID O	
281)	ALSI	324 P. 1015C-3A E	SVDA	1372	43M0DIF01			
282)	ALSI	32481015C-3A E	SWDA	1372			ULAM 0	
2831	ALS	36081015C-3B E	SUDA		OPTOT01	762CM	0	
284)	ALSAGFUBOREC	15C-38 E	SWDA	732	30SCREN01		0	
2853	ALSAGFDRORFC	-	SVDA	686	4		0	
2863	AI SAGEDRORFC	\$6001015C-3H F	SUDA	573	U IV JSE		0	
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187	ALSAGE UBUREC	١ د	40 mg	•	010040			
288)	ALSAGE DBOKE C-3	4	SWUA		SIKUPU	91CH	i	
289)	ALSAGFDBOREC	ш,	SWDA	0	SUSCS 0			
290)	ALSAGFDROREC	ш	SUDA	0	152C0L0R01		R 58	
291)	AL SAGF DROREC	ш	SWDA	0	20			
292)	AL	ш	SWDA	0	152M0ISC01		DRY	
293)	ALSAGFDBORFC-3	ш	SUDA	0	2LITHLO		RESID 0	
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308)	ALS	1336081015C-3B E	SWDA	457	153COLOR01		10R48 0	
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321	ALSAGF DBOREC	150-38	SHO	716	6CONSS0			
322	ALSAGF UDDREC	115C-38 E	SUDA	716	6MOISCO			
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324	AL	116C-3C E	43			1067CM		
325	AL	1338681316C-3C E	SUDA	1013	303CREN01		0	
326	AL SAGFOFOREC	38681616C-3C E	V	4	9SFILTO		0	
327	ALSAGEDROREC	016C-3C F	SLDA	832	11385 AL 01		0	
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### ### ### ### ### ### ### ### ### ##		1000	ALSAGT DEUREL	29		152	SHABLOD	2381			
13.66   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   10.06   13.86   10.06   13.86   10.06   10.06   13.86   10.06   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   10.06   13.86   13.86   13.86   13.86   13.8			ALSAGE UBUREC	6C-3C	SWDA	152	30505		2		
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ALSAGE DORNECT-3C	-	341)	SAGFDBOREC	60-30	SUDA	152	AL LINE			0 0	
ALSAFEDOREC-3C   1338681016C-3C   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1	-	342)	SAGFOBOREC	26-36	AUDA	305	200		2	0	
ALSAGE DORRECTOR 13386810166-35 ESUAR 305 135200.0801 1048 0  ALSAGE DORRECTOR 13386810166-35 ESUAR 305 135200.0801 1048 0  ALSAGE DORRECTOR 13386810166-35 ESUAR 305 135200.0801 10848 0  ALSAGE DORRECTOR 13386810166-35 ESUAR 457 155200.0801 1097860  ALSAGE DORRECTOR 13386810166-35 ESUAR 457 155200.0801 1097860  ALSAGE DORRECTOR 13386810166-35 ESUAR 457 155200.0801 1097860  ALSAGE DORRECTOR 13386810166-35 ESUAR 461 1097800.001 1097800.001 1097800.001 1097800.001 1097800.001 1097800.001 1097800.001 1097800.001 1097800.001 1097800.001 1097800.001 1097800.001 1097800.001 1097800.001 1097800.001 1097800.001 1097800.001 1097800.001 1097800.001 1097800.001 1097800.001 1097800.001 1097800.001 1097800.001 1097800.001 1097800.001 1097800.001 1097800.001 1097800.001 1097800.001 1097800.001 1097800.001 1097800.001 1097800.001 1097800.001 1097800.001 1097800.001 1097800.001 1097800.001 1097800.001 1097800.001 10	_	343)	SAGFDBOREC	75-74	4000	200	150UABLOUZ	1966		0	
ALSAFOROREC-3C 1338681016C-3C ESUDA 305 122CONSSO1 3T ACASTOROREC-3C 1338681016C-3C ESUDA 305 122CONSSO1 3T ACASTOROREC-3C 1338681016C-3C ESUDA 457 153481002 3481 C C C C C C C C C C C C C C C C C C C	~	344)	LSAGFDBOREC	3 2 3	4 0 0 0	000	10 5750261			0	
ALSAGE DORGE C3C 1338681016C-3C ESUDA 305 132CN03S01 ST 0  ALSAGE DORGE C3C 1338681016C-3C ESUDA 457 1514R1010  ALSAGE DORGE C3C 1338681016C-3C ESUDA 457 155CN0SS01 ST 0  ALSAGE DORGE C3C 1338681016C-3C ESUDA 457 155CN0SS01 ST 0  ALSAGE DORGE C3C 1338681016C-3C ESUDA 457 153CN0SS01 ST 0  ALSAGE DORGE C3C 1338681016C-3C ESUDA 457 153CN0SS01 ST 0  ALSAGE DORGE C3C 1338681016C-3C ESUDA 457 153CN0SS01 ST 0  ALSAGE DORGE C3C 1338681016C-3C ESUDA 457 153CN0SS01 ST 0  ALSAGE DORGE C3C 1338681016C-3C ESUDA 457 153CN0SS01 ST 0  ALSAGE DORGE C3C 1336881016C-3C ESUDA 457 153CN0SS01 ST 0  ALSAGE DORGE C3C 1336881016C-3C ESUDA 457 153CN0SS01 ST 0  ALSAGE DORGE C3C 1336881016C-3C ESUDA 457 153CN0SS01 ST 0  ALSAGE DORGE C3C 1336881016C-3C ESUDA 762 152CN0SS01 ST 0  ALSAGE DORGE C3C 1336881016C-3C ESUDA 762 152CN0SS01 ST 0  ALSAGE DORGE C3C 1336881016C-3C ESUDA 762 152CN0SS01 ST 0  ALSAGE DORGE C3C 1336881016C-3C ESUDA 762 152CN0SS01 ST 0  ALSAGE DORGE C3C 1336881016C-3C ESUDA 762 152CN0SS01 ST 0  ALSAGE DORGE C3C 1336881016C-3C ESUDA 762 152CN0SS01 ST 0  ALSAGE DORGE C3C 1336881016C-3C ESUDA 762 152CN0SS01 ST 0  ALSAGE DORGE C3C 1336881016C-3C ESUDA 762 152CN0SS01 ST 0  ALSAGE DORGE C3C 1336881016C-3C ESUDA 762 152CN0SS01 ST 0  ALSAGE DORGE C3C 1336881016C-3C ESUDA 914 1070CLORON 1  ALSAGE DORGE C3	_	345)	SAGFDBOREC	200	4000	200	152COLOR01		OR 4	0	
ALSAGFOROREC-3C 13386810146C-3C ESUDA 457 153401602 3481 CL 1346810146C-3C ESUDA 457 153401802 01 CL 0 13386810146C-3C ESUDA 457 153401802 01 CL 0 13386810146C-3C ESUDA 457 153401802 01 CL 0 13386810146C-3C ESUDA 457 153401803 01 ST 0 134881016C-3C ESUDA 457 153401803 01 ST 0 134881016C-3C ESUDA 457 153401803 01 ST 0 134881016C-3C ESUDA 457 153401802 01 CL 0 1348861016C-3C ESUDA 457 1534181002 3991 ESS10 0 1438681016C-3C ESUDA 457 1534181002 2591 CL 0 1438691086C-3C 1338681016C-3C ESUDA 457 15411810 1 144891002 2591 CL 0 1438691086C-3C 1338681016C-3C ESUDA 457 15411810 1 144891006C-3C 1338681016C-3C ESUDA 457 15411810 1 14489100C 2591 CL 0 14489100C 2591 CSUDA 457 15411810 1 14489100C 2591 CSUDA 457 154118100C 2591 CSUDA 457 15411810 1 14489100C 2591 CSUDA 457 154118100C 2591 CSUDA 457 15411810 1 14489100C 2591 CSUDA 457 15411810 1	_	-	SAGEDROPEC	30-30	× 0 × 0	202	152CONSS01		ST	0	
13.06.01166-36   ESUDA   305 152L17HL01   RESTD   ALSAF DODREC-3C   13.306.01106-3C   ESUDA   457 155.00.00001   1004-80   13.306.01106-3C   ESUDA   457 155.00.00001   1004-80   13.306.01016-3C   ESUDA   450 152.00.0001   1004-80   13.306.01016-3C   ESUDA   450 152.00.0001   1004-80   13.306.01016-3C   ESUDA   762 152.00.0001   1004-80   13.306.01016-3C   ESUDA   107.00.0000   10.306.00000   13.306.01016-3C   ESUDA   107.00.0000   10.306.0000   10.306.0000   10.306.0000   10.306.0000   10.306.0000   10.306.0000   10.306.0000   10.306.0000   10.306.0000   10.306.0000   10.306.0000   10.306.0000   10.306.0000   10.306.0000   10.306.0000   10.306.0000   10.306.0000   10.306.0000   10.306.0000   10.306.0000   10.306.0000   10.306.0000   10.306.0000   10.306.0000   10.306.0000   10.306.0000   10.306.0000   10.306.0000   10.306.0000   10.306.0000   10.306.0000   10.306.0000   10.306.0000   10.30	-	-	CAGEDOOPE	25-36	SEDA	305	152M01SC01		DRY	0	
ALSAFE BOREC-3C  13366 810166-3C ESWDA 457 1554MBL002 346 L  ALSAFE BOREC-3C  13366 810166-3C ESWDA 457 155COOR01  13366 810166-3C ESWDA 457 155LITHL01  13366 810166-3C ESWDA 457 155LITHL01  13366 810166-3C ESWDA 467 155LITHL01  13366 810166-3C ESWDA 762 152COOR01  13366 810166-3C ESWDA 914 107COOR0501  1400000000000000000000000000000000	-	. 0	SACE DECEMBER	26-36	SUDA	305	152LITHL01		-	0	
ALSAFE DRORECT-3C   1338 681016C-3C ESWDA   457 155COLOR01   10848   0	•	0 0	SAGEDOORE	9C-3C	SWDA	457	153HABL002	4			
ALSAFE PROPRICE-3C	•	n .	SAGFUBUREC	5C-3C	SWDA	457	3050505 01		5		
### SAME PROPRIET3C	• •	250	SAGFDBOREC	SC-3C	SUDA	457	1530010801				
ALSAGFORGEC-3C 1338681016C-3C ESUDA 457 153801SC01 LM CALSAFORGEC-3C 1338681016C-3C ESUDA 457 153801SC01 LM CALSAFORGEC-3C 1338681016C-3C ESUDA 610 15220NS01 STT 0 1358681016C-3C ESUDA 762 152NABLOOC 258L CL 0 1358681016C-3C ESUDA 762 152NBLOOC 258L CL 0 1358681016C-3C ESUDA 762 16C-3C ESUDA 762 16C-3		351)	SAGFDBOREC	SC-3C	_	457	153CONSC01				
ALSAGF DROREC-3C  13366 NIDIGC-3C SWOA  ALSAGF DROREC-3C  ALSAGF DROREC-3C  13366 NIDIGC-3C SWOA  ALSAGF DROREC-3C  13366 NIDI	-	352)	LSAGFDBOREC	SC-3C		457	15 TWO TO TO		- :		
ALSAFF DBOREC-3C  1338681016C-3C  ESWDA  10 152COLORD1  10 10 10 10 10 10 10 10 10 10 10 10 10 1	~	353)	LSAGF DBOREC-3	75-75		200	1036013601			0	
ALSAGF DBOREC-3C  ALSAGF BBOREC-3C  ALSAGF BBORE	~	354)	LSAGFOBORFC	200			133C11HC01		ESI	0	
ALSAGE DRORECTOR	~	355)	LSAGFORORFC	2000		019	152HABL002	39BL		0	
ALSAFDBOREC-3C 1338681016C-3C ESWDA 610 152CONSSO1 ST 0  ALSAFDBOREC-3C 1338681016C-3C ESWDA 610 152L11HL01  ALSAFDBOREC-3C 1338681016C-3C ESWDA 610 152L11HL01  ALSAFDBOREC-3C 1338681016C-3C ESWDA 762 152USCS 01 10TR660  ALSAFDBOREC-3C 1338681016C-3C ESWDA 762 152CONSSO1 ST 0  ALSAFDBOREC-3C 1338681016C-3C ESWDA 762 152CONSSO1 ST 0  ALSAFDBOREC-3C 1338681016C-3C ESWDA 762 152M17HL010  ALSAFDBOREC-3C 1338681016C-3C ESWDA 762 152M17HL010  ALSAFDBOREC-3C 1338681016C-3C ESWDA 762 152M17HL010  ALSAFDBOREC-3C 1338681016C-3C ESWDA 914 107USCS 01 CL 0  ALSAFDBOREC-3C 1338681016C-3C ESWDA 1021 46MBL002  ALSAFDBOREC-3C 133881016C-3C ESWDA 1021 46MBL002  ALSAFDBOREC-3C 133881016C-	_	356)	SAGFORORFC-T	1 - 3 C E	MONS	210	152COLOR01		10YR66	0	
ALSAGE BOREC-3C  ALSAGE	-	3573	SAGEDROR	1-30	SHUA	210	152CONSS01		ST	0	
ALSAGE DBOREC - 3C	_	3583	SAGFOROR	10-36	MONS	210	152M01SC01		5	0	
ALSAGF DORRECTOR 1338681016C-3C ESWDA 762 15204BL002 25BL CL CALSAGF DORRECTOR 1338681016C-3C ESWDA 762 152005C0 1 107R660 25.00 1 107R67 25.00	-	3591	SAGEDBORFC-7	1-3C E	SADA	210	152LITHL01		ESI	0	
ALSAGF DRORECTOR	-	3603	SACEDBOOLS	C-3C E	SUDA	162	152HABL002	25BL		0	
ALSAGF DRORECTOR 1336681016C-3C ESWDA 762 152COLOR01 107R660  ALSAGF DRORECTOR 1336681016C-3C ESWDA 762 152COLOR01 107R660  ALSAGF DRORECTOR 1336681016C-3C ESWDA 762 152L17HL01 RESID 0  ALSAGF DRORECTOR 1336681016C-3C ESWDA 914 107DCLOR01 27BL CL 0  ALSAGF DRORECTOR 1336681016C-3C ESWDA 914 107DCLOR01 27BL CL 0  ALSAGF DRORECTOR 1336681016C-3C ESWDA 914 107DCLOR01 27BL CL 0  ALSAGF DRORECTOR 1336681016C-3C ESWDA 914 107DCLOR01 1 LM 0  ALSAGF DRORECTOR 1336681016C-3C ESWDA 914 107DCLOR01 1 LM 0  ALSAGF DRORECTOR 1336681016C-3C ESWDA 1021 46UDCS 01 CL 0  ALSAGF DRORECTOR 1336681016C-3C ESWDA 1021 46UDCS 01 CL 0  ALSAGF DRORECTOR 1336681016C-3C ESWDA 1021 46UDCS 01 CL 0  ALSAGF DRORECTOR 1336681016C-3C ESWDA 1021 46UDCS 01 CL 0  ALSAGF DRORECTOR 1336681016C-3C ESWDA 1021 46UDCS 01 CL 0  ALSAGF DRORECTOR 1336681016C-3C ESWDA 1021 46UDCS 01 CL 0  ALSAGF DRORECTOR 1336681016C-3C ESWDA 1021 46UDCS 01 CL 0  ALSAGF DRORECTOR 1336681016C-3C ESWDA 1021 46UDCS 01 CL 0  ALSAGF DRORECTOR 1336681016C-3C ESWDA 1021 46UDCS 01 CL 0  ALSAGF DRORECTOR 1336681016C-3C ESWDA 1021 46UDCS 01 CL 0  ALSAGF DRORECTOR 133681016C-3C ESWDA 1021 46UDCS 01 CL 0  ALSAGF DRORECTOR 133681016C-3C ESWDA 1021 46UDCS 01 CL 0  ALSAGF DRORECTOR 133681016C-3C ESWDA 1021 46UDCS 01 CL 0  ALSAGF DRORECTOR 133681016C-3C ESWDA 1021 46UDCS 01 CL 0  ALSAGF DRORECTOR 133681016C-3C ESWDA 1021 46UDCS 01 CR 01		1611	SACE DEPORT	C-3C	SUDA	162	152USCS 01		CL	0	
ALSAGF BOOKEC - 3C  1338681016C - 3C  1538681016C - 3C  1588081016C - 3C  1588081016		16.55	SAGREDOREC	38681016C-3C E	SUDA	162	152COLOR01			0	
ALSAGF DROREC - 3C  1338681016C - 3C  ESWDA 762 152H7HL01  RESID 0  ALSAGF DROREC - 3C  1338681016C - 3C  ESWDA 914 107H3C102  ALSAGF DROREC - 3C  1338681016C - 3C  133868101		2000	SAGEDBOREC		SUDA	162	152CONSS01				
ALSAGF DBOREC - 3	•	1040	SAGFUROREC			162	152M01SC01				
ALSAGF DHOREC-3C  1338681016C-3C ESWDA 914 107HABLOOZ  ALSAGF DHOREC-3C  1338681016C-3C ESWDA 914 107HABLOOZ  ALSAGF DHOREC-3C  1338681016C-3C ESWDA 914 107COLOR01  2578460  ALSAGF DHOREC-3C  1338681016C-3C ESWDA 914 107CONSSSSSSSSSSSSSSSSSSSSSSSSSSSSSSSSSSSS		364)	LSAGFDBORE	_	SUDA	162	1521 1THI 01		Dreta		
ALSAGF DBOREC-3C  15386 B1016 C-3C  ESWDA 914 1070 SCS 01  CL 0  ALSAGF DBORE C-3C  15386 B1016 C-3C  ESWDA 914 1070 SCS 01  LM 0  ALSAGF DBORE C-3C  15386 B1016 C-3C  ESWDA 914 1070 SCS 01  LM 0  2557 460  ALSAGF DBORE C-3C  15386 B1016 C-3C  ESWDA 914 1070 SCS 01  LM 0  ALSAGF DBORE C-3C  15386 B1016 C-3C  ESWDA 1021 46 HABLOO2  CL 0  ALSAGF DBORE C-3C  15386 B1016 C-3C  ESWDA 1021 46 HOSCS 01  CL 0  CL 0  CL 0  ALSAGF DBORE C-3C  15386 B1016 C-3C  ESWDA 1021 46 COLOR 01  ESYPAGO  ALSAGF DBORE C-3C  15386 B1016 C-3C  ESWDA 1021 46 COLOR 01  ESYPAGO  ALSAGF DBORE C-3C  15386 B1016 C-3C  ESWDA 1021 46 COLOR 01  ESYPAGO  ALSAGF DBORE C-3C  15386 B1016 C-3C  ESWDA 1021 46 COLOR 01  ESYPAGO  ALSAGF DBORE C-3C  15386 B1016 C-3C  ESWDA 1021 46 COLOR 01  ESYPAGO  ALSAGF DBORE C-3C  15386 B1016 C-3C  ESWDA 1021 46 COLOR 01  ESYPAGO  ALSAGF DBORE C-3C  15386 B1016 C-3C  ESWDA 1021 46 COLOR 01  ESYPAGO  ALSAGF DBORE C-3C  15386 B1016 C-3C  ESWDA 1021 46 COLOR 01  ESYPAGO  ALSAGF DBORE C-3C  1528 B1016 C-3C  ESWDA 1021 46 COLOR 01  ESYPAGO  ALSAGF DBORE C-3C  1528 B1016 C-3C  ESWDA 1021 46 COLOR 01  ESYPAGO  ALSAGF DBORE C-3C  1528 B1016 C-3C  ESWDA 1021 46 COLOR 01  ESYPAGO  ALSAGF DBORE C-3C  1528 B1016 C-3C  ESWDA 1021 46 COLOR 01  ESYPAGO  ALSAGF DBORE C-3C  1528 B1016 C-3C  ESWDA 1021 46 COLOR 01  ESYPAGO  ALSAGF DBORE C-3C  1528 B1016 C-3C  ESWDA 1021 46 COLOR 01  ESYPAGO  ALSAGF DBORE C-3C  1528 B1016 C-3C  ESWDA 1021 46 COLOR 01  ESYPAGO  ALSAGF DBORE C-3C  1528 B1016 C-3C  ESWDA 1021 46 COLOR 01  ESYPAGO  ALSAGF DBORE C-3C  1528 B1016 C-3C  ESWDA 1021 46 COLOR 01  ESYPAGO  ALSAGF DBORE C-3C  1528 B1016 C-3C  ESWDA 1021 46 COLOR 01  ESYPAGO  ALSAGF DBORE C-3C  1528 B1016 C-3C  ESWDA 1021 46 COLOR 01  ESYPAGO  ALSAGF DBORE C-3C  1528 B1016 C-3C  ESWDA 1021 46 COLOR 01  ESYPAGO  ALSAGF DBORE C-3C  1528 B1016 C-3C  ESWDA 1021 46 COLOR 01  ESYPAGO  ALSAGF DBORE C-3C  1038 B1016 C-3C  ESWDA 1021 46 COLOR 01  ESYPAGO  1030 B1016 C-3C  ESWDA 1021 46 COLOR 01  ESYPAGO  1021 46 COLOR 01  ESYPAGO  1030 B1016 C-3C  ESWDA 10	_	365)	AGF DHOREC	30	SUDA	41.0	107HABIODO	101	016370		
ALSAGF DEOREC-3C  ACTUMINICAL ALSAGF DEOREC-3C  ACTUMINICAL ALSAGF	_	366)	AGFDBOREC	30			20070000	18/		0	
ALSAGFDROREC-3C  ALSAGFBROREC-3C  ACTION OF ALSAGFBROREC-3C  ACTION OF ALSAGFBROREC-3C  ACT	_	367)	SAGFDEORFF	, ,			10 5050 01			0	
ALSAGF DRORECTS C. 133R6 E1016C-3C ESWDA 914 107MOISCOI . LM 0  ALSAGF DRORECTS C. 133R6 E1016C-3C ESWDA 914 107CONSS 01 ST 0  ALSAGF DRORECTS C. 133R6 E1016C-3C ESWDA 1021 46HABLOOZ 20BL CL 0  ALSAGF DRORECTS C. 133R6 B1016C-3C ESWDA 1021 46COLOR01 25FP460  ALSAGF DRORECTS C. 133R6 B1016C-3C ESWDA 1021 46COLOR01 ST 0  ALSAGF DRORECTS C. 133R6 B1016C-3C ESWDA 1021 46COLOR01 ST 0  ALSAGF DRORECTS C. 133R6 B1016C-3C ESWDA 1021 46COLOR01 ST 0  ALSAGF DRORECTS C. 133R6 B1016C-3C ESWDA 1021 46COLOR01 ST 0  ALSAGF DRORECTS C. 133R6 B1016C-3C ESWDA 1021 46COLOR01 ST 0  ALSAGF DRORECTS C. 133R6 B1016C-3C ESWDA 1021 46COLOR01 ST 0  ALSAGF DRORECTS C. 133R6 B1016C-3C ESWDA 1021 46COLOR01 ST 0  ALSAGF DRORECTS C. 133R6 B1018 B1	~	368)	SACFORDEC	36		114	107COLOR01		846	0	
ALSAGF DRORECTOR 1354681016C-3C ESWDA 914 107CONSSG1 ST 0  ALSAGF DRORECTOR 1358681016C-3C ESWDA 919 107LITHL01 RESTD 0  ALSAGF DRORECTOR 1358681016C-3C ESWDA 1021 4640SCS 01 CL 0  ALSAGF DRORECTOR 1358681016C-3C ESWDA 1021 4640SCS 01 CL 0  ALSAGF DRORECTOR 1358681016C-3C ESWDA 1021 4640SCS 01 CL 0  ALSAGF DRORECTOR 1358681016C-3C ESWDA 1021 4640SS01 ST 0  ALSAGF DRORECTOR 1358681016C-3C ESWDA 1021 4640SS01 CL N 0  ALSAGF DRORECTOR 1358681016C-3C ESWDA 1021 4640SS01 CL N 0  ALSAGF DRORECTOR 1358681016C-3C ESWDA 1021 4640SCR N 0  ALSAGF DRORECTOR 12580181035F-31 ESWDA 1021 4640SCR N 0  ALSAGF DRORECTOR 12580181035F-31 ESWDA 1021 610SCR N 0  ALSAGF DRORECTOR 12580181035F-31 ESWDA 1021 4650S01	-	1601	CACEDOOC	3C F		114	107M01SC01		E .	0	
ALSAGF DEOREC-3C  1338681016C-3C ESWDA 1021 46HABLO02  ALSAGF DEOREC-3C  1338681016C-3C ESWDA 1021 46HABLO02  ALSAGF DEOREC-3C  1338681016C-3C ESWDA 1021 46COLOR01  ALSAGF DEOREC-3C  1338681016C-3C			SHOT UPOR CL	3C E		114	107CONSS 61		_	•	
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430) ALSAGFI	ALSAGFDUOREP-32	12917810364-32	ESHDA	722	25FILL 01		0
451) ALSAGF	ALSAGF DRCKEP-32	12917810365-32	ESWOA	250	472SCRENDI	8	0
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434) ALSAGF	ALSAGE DROPEP-32	12717H13364-32	ESTUA	6.	616R0UT31		1
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